# Dutteville Landing-2017



# Butteville Landing - 2024



#### DEPARTMENT OF THE ARMY

CORPS OF ENGINEERS, PORTLAND DISTRICT P.O. BOX 2946 PORTLAND, OREGON 97208-2946

July 22, 2019

Regulatory Branch Corps No.: NWP-2018-135

Mr. Ben Williams Friends of Historic Butteville P.O. Box 506 Donald, Oregon 97020 Ben.Williams@liturgica.com

Dear Mr. Williams:

The U.S. Army Corps of Engineers (Corps) received your request for a Department of the Army permit to construct a dock. The project is located on the Willamette River (River Mile 42.9) at Butteville Street NE in Butteville, Marion County, Oregon at Latitude and Longitude 45.262550, -122.843822. This "Letter of Permission" (LOP) permit authorizes your project as depicted on the enclosed drawings (Enclosure 1). The time limit for completing the work authorized by this LOP ends 5 years from the date of this letter.

The work includes construction of a dock with steel anchor pile, an aluminum access gangway, and concrete abutment. In-water work in the Willamette River includes a floating dock and five, 16-inch diameter anchor pilings. The aluminum grated gangway above water will span between the dock and land for access. The encapsulated float drum dock with Eco-Grate 62 Fibregrate decking and gangway will be fabricated off site. The gangway will be a total of 118 feet long and four feet wide, and the floating dock will be 36 feet long and six feet wide. Work will be conducted from a floating barge secured by pilings. Pilings will be placed with vibratory hammer. The gangway will be set in place and secured with pilings at the top of bank.

In order for this LOP authorization to be valid, you must ensure the work is performed in accordance with the enclosed Letter of Permission General Conditions (Enclosure 2) and the following special conditions:

a. The permittee understands and agrees that, if future operations by the United States require the removal, relocation, or other alteration, of the structure or work herein authorized, or if, in the opinion of the Secretary of the Army or his authorized representative, said structure or work shall cause unreasonable obstruction to the free navigation of the navigable waters, the permittee will be required, upon due notice from the U.S Army Corps of Engineers, to remove, relocate, or alter the structural work or

obstructions caused thereby, without expense to the United States. No claim shall be made against the United States on account of any such removal or alteration.

- b. If human remains or cultural resources are discovered during the performance of the authorized work the permittee shall implement the Inadvertent Discovery Plan procedures (Enclosure 3) and immediately notify the U.S. Army Corps of Engineers, Portland District, Regulatory Branch.
- c. Permittee shall have a Qualified Professional Archeologist meeting the requirements of 36 Code of Federal Regulations Part 61 Appendix A present to monitor for archeological objects during all portions of the project-related earthmoving disturbances, specifically for installation of the concrete walkway and excavation for the new concrete abutments behind the proposed pile.
- d. Within 90 days of completing earthmoving disturbances, the permittee shall submit a brief monitoring report prepared by the professional archeologist(s) that performed the monitoring by e-mail to: cenwp.notify@usace.army.mil and orshpo.clearance@oregon.gov that describes the monitoring activities. The monitoring report shall include the following components: the permit number; name(s) and qualification(s) of archeologist(s) that did the monitoring; topographic and aerial map showing area monitored; dates of monitoring; description of activities monitored to include depth; description of cultural material identified or lack thereof; and photos of the monitoring activities.
- e. Permittee shall fully implement all applicable Proposed Design Criteria (PDC) of the SLOPES IV In-water Over-water Structures programmatic opinion. A detailed list of the PDC's are enclosed (Enclosure 4). The PDC's included with the SLOPES notification for the project include numbers: 5-7, 12-13, 17-18, 21, and 30-31.
- f. Permittee shall fully plant all areas immediately following completion of construction as shown in the Planting Plan (Enclosure 1, Pages 7-9).
- g. All in-water work shall be performed during the in-water work period(s) of June 1 October 31 to minimize impacts to aquatic species. Exceptions to these time periods require specific approval from the Corps and the National Marine Fisheries Service.

The requirements of the Endangered Species Act were met through a programmatic biological opinion as listed in the special condition above. The complete text of the biological opinion is available for your review at http://www.nwp.usace.army.mil/Missions/Environment/SLOPES.aspx. Please note, you must submit a SLOPES *Action Completion Report* form which is provided in Enclosure

4. We have reviewed your project pursuant to the requirements of the Endangered Species Act, the Magnuson-Stevens Fishery Conservation and Management Act and the National Historic Preservation Act. We have determined the project complies with the requirements of these laws provided you comply with all of the permit general and special conditions.

The Willamette River is a water of the U.S. If you believe this is inaccurate, you may request a preliminary or approved jurisdictional determination (JD). If one is requested, please be aware that we may require the submittal of additional information to complete the JD and work authorized in this letter may not occur until the JD has been completed.

If you object to any terms or conditions of this LOP, you may request an administrative appeal under our regulations (33 CFR Part 331) as described in the enclosed *Notification of Administrative Appeal Options and Process and Request for Appeal* form (Enclosure 5).

LOP General Condition 6 requires you to obtain the signatures(s) of the new owner(s) if you sell the property associated with this permit in order to transfer the permit to the new owner. For your convenience, the enclosed *Transfer of Permit* form (Enclosure 6) can be prepared and submitted to document the permit transfer.

This LOP permit is based on the project description and construction methods provided in your permit application. If you propose changes to the project, you must submit revised plans to this office and receive our approval of the revisions prior to performing the work. Failure to comply with all terms and conditions of this LOP invalidates this authorization and could result in a violation of Section 404 of the Clean Water Act and/or Section 10 of the Rivers and Harbors Act. You must also obtain all local, State, and other Federal permits that apply to this project.

Upon completing the authorized work, you must fill out and return the enclosed *Compliance Certification* form (Enclosure 7). We would like to hear about your experience working with the Portland District, Regulatory Branch. Please complete a customer service survey form at the following address: http://corpsmapu.usace.army.mil/cm\_apex/f?p=regulatory\_survey.

If you have any questions regarding this LOP, please contact Ms. Carrie Bond at the letterhead address, by telephone at (503) 808-4387, or e-mail: Carrie.L.Bond@usace.army.mil. This permit becomes effective when the Federal official, designated to act for the Secretary of the Army, has signed below.

FOR THE COMMANDER, AARON L. DORF, COLONEL, CORPS OF ENGINEERS, DISTRICT COMMANDER:

For: William D Abadie Chief, Regulatory Branch

**Enclosures** 

CC:

Oregon Department of State Lands (De Blasi)
Oregon Department of Environmental Quality (401applications@deq.state.or.us)
Flowing Solutions, LLC (Andrew Jansky, andrew@flowingsolutions.com)

By email from: Marc Liverman - NOAA Federal marc.liverman@noaa.gov

To: Bond, Carrie L NWP Carrie.L.Bond@usace.army.mil

RE: SLOPES IWOWS: Butteville Landing River Access, Over-water Structures & Stormwater, Willamette River, Marion Co

July 9, 2019

Ms. Bond:

I read the notification form submitted to NMFS by the Corps on Mar 26, 2018 requesting that NMFS review and confirm the action named above is consistent with the SLOPES IWOWS opinion issued to the Corps on Apr 5, 2012. The proposed action was found inconsistent with the SLOPES opinion on Jul 17, 2019. This review is based on a revised project submittal, received by NMFS on Jun 13, 2019.

The proposed project is likely to adversely affect ESA-listed species, designated critical habitat, and essential fish habitat through the following activities:

- In-water construction
- Piling installation
- Habitat modification / New floats
- Stormwater

Based on information submitted by the Corps and the Friends of Historic Butteville Landing and their consultants, the proposed action is consistent with the SLOPES IWOWS opinion for:

- Project design
- In-water work period
- Piling Installation
- Heavy equipment use
- Stormwater Management
- New Floats
- All other relevant project design criteria for construction practices

I confirm this action meets the conditions of the SLOPES IWOW programmatic biological opinion issued on April 5, 2012. A copy of all review materials is on file at NMFS' Oregon-Washington Coastal Office. Please note that the opinion requires the Corps to submit a project completion report for this project within 60-days of end of project activities.

Reinitiation of consultation on this action is required and shall be requested by the Corps where discretionary Federal involvement or control over the action has been retained or is authorized by law and (a) the amount or extent of taking specified in the Incidental Take Statement is exceeded, (b) new information reveals effects of the action that may affect listed species or critical habitat in a manner or to an extent not previously considered, (c) the identified action is subsequently modified in a manner that has an effect to the listed species or critical habitat that was not considered in the biological opinion; or (d) a new species is listed or critical habitat designated that may be affected by the identified action (50 CFR 402.16).

My point of contact for this response is Brad Rawls, who can be reached at 503-230-5414 or by email at <a href="mailto:brad.rawls@noaa.gov">brad.rawls@noaa.gov</a>.

Marc Liverman Willamette Branch Chief West Coast Region NOAA Fisheries Service



Parks and Recreation Department

State Historic Preservation Office 725 Summer St NE Ste C Salem, OR 97301-1266 Phone (503) 986-0690 Fax (503) 986-0793 www.oregonberitage.org



April 20, 2018

Ms. Carrie Bond USACE - Portland PO Box 2946 Portland, OR 97208-2946

RE: SHPO Case No. 18-0412

NWP-2018-135, Butteville Landing River Access

New path, sign, plantings, dock

Butteville St (3S 1W 32), Butteville, Marion County

#### Dear Ms. Bond:

Our office recently received your application for the project referenced above. We have reviewed your application and have concerns regarding potential impacts to site 35MA394 resulting from the proposed project. Your application states that the proposed gangway-to-dock will be placed on top of site 35MA394, which while its eligibility to the National Register (NR) is currently unevaluated, the original recorder believed that the site should be considered eligible to the NR. With this in mind, what will be the potential impact on 35MA394, both directly and indirectly? Our office has a few questions regarding the project's design. They include: 1) will the construction of the gangway directly affect the existing foundation in any way? The drawings we have seen appears to show the gangway being placed above the old foundation but your letter suggests that it will be placed directly on top of it; 2) Will buried artifacts be disturbed during the construction of the pile that will be placed on land above the existing foundation?; 3) the engineering sketch suggests that new concrete abutments will be installed behind the proposed pile that will require ground disturbance. Our office believes that it is important that an archaeologist be on site to monitor the construction of the gangway and placement of any structures to be built/placed on land. If the gangway is to actually be built directly on top of the existing foundation, our office will want to receive sufficient information prior to construction that will assure us that no adverse effect to the structure will occur. If the gangway is built above the existing foundation, with no direct contact, we are less concerned about potential effect to the structure. Our office understands the liability such a foundation must have with people playing on the structure and we understand the efforts being spent to construct a new dock in the area. However, we want to be sure that the proposed construction does not result in unexpected impacts to site 35MA394 or other previously unidentified cultural remains. Upon completion of the construction, our office will expect to receive a copy of a monitoring report along with an updated archaeological site form that will include information on the changes to the surrounding landscape.

Under state law (ORS 358.905-955 & ORS 97.740) archaeological sites, objects and human remains are protected on both public and private land in Oregon. If project impacts and the degree/type of required ground disturbance changes from that outlined in your report, further consultation with our office will be required before proceeding with the proposed activity. If you have any questions regarding any future discovery, or this letter, feel free to contact our office.

Sincerely,

Dennis Griffin, Ph.D., RPA

Ensur Juffer

State Archaeologist (503) 986-0674 dennis.griffin@oregon.gov

cc: Michael DeBlasi, DSL

#### Site record: 17-98-1 (Butteville Landing)

Admin/Tyne/Location

Admin/ Lype/Location					
Smithsonian	Alt Site #s 17-98-1				
Site name Butteville Landing	Form type New				
Managing office Private	County Marion				
NRHP status Recommended Eligible	Role fieldworker	Date September 25, 2017	Author Matt Goodwin		
Site type scatter	Owner Marion County		***		
Features none	Cultural periods Depression/WWII, Historic, Post WWII				
Length 75	Width 25	Units meter	Area 0.43 acres		
Depth NA					
General age Historic period					
Township 3S	Range 1W	Section 32	⅓s se-sw-se	Meridian Willamette	
Type centerpoint	East 5012125	North 512273	Method GPS <1m	Zone 10	Datum 83
Map name/year Sherwood 7.5'	Revision year 2014				

#### Access Description:

From the intersection of SW Boones Ferry Rd. and Wilsonville Rd. in the city of Wilsonville, drive west on Wilsonville Rd. for 0.1 miles. Turn right onto the I-5 South on ramp and merge on to I-5. Travel south on I-5 for 1.2 miles and take exit 282A on to the Portland-Hubbard Hwy. Continue south for 0.7 miles on the Portland-Hubbard Hwy. to Arndt Rd. Turn right onto Arndt road and travel west for 3.5 mile to the town of Butteville. Turn left on Butteville Rd. NE and drive 0.1 miles to Butte St. NE. Turn right onto Butte St. NE and park. Butte St. NE continues a two-pronged driveway leading to two residences, Walk straight at the fork for approximately 65 m along a primitive dirt trail to the Butteville Landing site, on the southern shore of the Willamette River.

#### Environmental data

Diffi Oninchtal data	
Province Willamette	
Valley	
Basin Lower Willamette	
Subbasin	
Drainage name	
Willamette River	
Elevation 100 feet	
Aspect north	
Depositional	
environment alluvial	
Soil Description Cloquato	silt loam, 0 to 3 percent slopes
Culturally signification	

vegetation ferns, cedar Culturally signification vegetation description none					
Water source name Willamette River	Type river	Stream type perennial	Stream class	Distance 0 m	Direction 0 deg

#### Site setting:

This site is in the Willamette River watershed of the Willamette Valley physiographic province in Marion County, Oregon (Figures 1-2). The Willamette Valley is part of the pine-oak-fir (*Pinus-Quercus-Pseudotsuga*) zone (Franklin and Dyrness 1988) ecological zone. The site is on the shore of the Willamette River and the community of Butteville is immediately southwest of the site. The Butteville Landing site is on a Marion County street right-of-way and is managed and administered by the county. Most of the surrounding area is developed as residential and commercial property. The site lies on the Willamette River shoreline, rising up along the terrace tread in southeasterly direction approximately 75 meters to the top of the terrace. Portions of the site, including documented wood piling and concrete features are either seasonally or perennially inundated.

Site Description

Site Description			
(Dates of use)	To modern	BP/AD/BC	Method historic maps,
From 1851	1	AD	background review and
			feature typology
Artifacts present:	Artifact quantity:	Estimated counts	Estimated counts
none observed	na	historic	prehistoric na
		na	

Willamette CRA archaeologists were contracted to document the structural remains and features at the Butteville landing site by the Friends of Historic Butteville in anticipation of a proposed river access improvement project. The site consists of a series of concrete structural remains/ruins, partially buried iron I-beams and the remains of wood pilings/piers (Figures 3-10) along the Willamette River shoreline and up the terrace tread within the 60 foot wide right-of-way of Butte Street NE. The documented features occur over an area measuring 75 m (southeast/northwest) by 25 m (northeast/southwest). Site boundaries are based on a combination of the width of the Butte St. NE right-of-way, extent of observed features, and water. While ground visibility was limited, archaeologists did not observe any historic-period artifact on the ground surface within the site. The extent of the Butte St. NE right-of-way forms the southwest and northeast boundaries of the site. The last of a series of partially buried iron beams marks the southwest boundary, near the paved roadway/driveway. In the northeast, the river, beyond the point of the last observable wood pier remnant, is the northeastern site boundary.

A total of 4 concrete features, that appear to be in-situ, were observed at the Butteville Landing site. Additionally, WillamtteCRA archaeologists noted approximately 20-25 large pieces of concrete rubble/debris, ranging in size from 12 ft. by 6 ft. to 2 ft. by 1 ft. Eight wood piling remnants, with at least some portion of the piling extending above the Willamette River water surface, were documented and mapped. Along the southwest margin of the site, a partially collapsed concrete structure/foundation extends from the edge of the terrace riser downslope into the water (see Figures 4, 6-8). The remains of the feature measure approximately 40 ft. on the long axis (NW-SE) by 15 ft, on wide (NE-SW axis). The structure appears to have been composed of three rectangular segments, with the largest being the farthest northwest segment (at the waters edge). Dirt, debris and water fill the various portions of the feature. The walls of the feature at their tallest (in the larger segment near the water) are 9 ft. 6 in. in height (see Figure 6). The concrete walls of the feature are not uniform in thickness, but are generally 12-14 in. wide. When viewing the walls from the side striations, 12-16 in. tall, are apparent that likely indicate a method of construction that involved pouring the concrete in segments or layers (see Figure 6). The concrete aggregate used in construction of the walls is comprised of rounded pebbles and sand. Remnants of large bolts, some with nuts and washers still attached, protrude from the concrete along some sections of the walls (see Figure 8). The bolts, generally, are ¼ in. thick and protrude 15-16 in. outward from the concrete. Extant nuts are 2 by 2 in, and the washers observed were 4 in, in diameter, Rubble from collapsed wall segments is apparent throughout the feature and along all sides.

Two concrete wall remnants, of similar material and construction as the larger feature, are located to the northeast along the water's edge. The first is approximately 21 ft. northeast of the larger feature and extends a distance of 14 ft. (NW-SE) along the terrace riser, downslope into the water (see Figures 4, 5 and 9). The second wall segment is approximately 30 ft. northeast of the larger feature and extends a distance 9 ft. (NW-SE) along the terrace riser, downslope into the water. Collapsed portions of the walls, in the form of concrete rubble, are littered along the terrace riser.

A fourth extant concrete feature, a square concrete footer or pier, is located approximately 20 ft. northeast of the larger feature near the top of the terrace riser (see Figures 4 and 10). The concrete footer measures 2 ft. by 2 ft. and rises 3 ft. 6 in. above the current ground surface. A large bolt, with attached nut and washer, of the same make and material as those on the larger feature is centered on the top of the footer/pier.

In addition to the concrete structural remains and the wood pilings, WillametteCRA archaeologists documented a series of iron beams and two survey markers/monuments. The beams extend up the Butte St. NE right-of-way toward the extant road and the top of the secondary terrace (see Figure 3). The beams are approximately 6 in. wide and extend, generally, about 3-4 ft. above the ground surface. A United States Coast and Geodetic Survey (USCGS) marker was documented, embedded in the southeastern-most concrete wall of the large feature and a Marion County Public Works marker was noted along the northeastern edge of the right-of-way. The USCCGS survey marker has been badly damaged and not all of the lettering is legible, so a date for the marker could not be made out.

The town of Butteville was platted in the late 1840s and was granted a United States Post Office in 1850 (McArthur and McArthur 2003). The first steamboat arrived at the Butteville landing in 1851 and for the next 20 years residents of Butteville and the surrounding communities used the riverboats that stopped at the landing to transport goods to market (Corning 1973) In 1873 the Oregon and California Railroad line was completed through the communities of Canby and Aurora, to the east of Butteville, and in 1908 the Oregon Electric line was completed, crossing the Willamette River at Wilsonville. The completion of these railroad lines led to a decline in the use of the river for the transport for goods and people. A series of ferries continued to operate from the Butteville Landing into the middle part of the 20th century (Query 2008). The completion of Interstate 5 and the opening of the Boone Bridge at Wilsonville in 1954 led to the decline of the ferries on this portion of the Willamette River.

Review of historic-period maps did not indicate any structures in the location of the recorded features; however, maps as far back as the 1851 General Land Office Map (GLO) depict a ferry crossing at this location (General Land Office 1851). Historic period photos and drawings accessed for this site record depict several iterations of docks, piers and other structures at the site of the Butteville Landing spanning the mid-late 19th and early 20th centuries (Figures 11-15). While it is not completely clear if the features recorded on this site record coincide with any of the structures depicted in the historic-period photos, many similarities in shape and scale can be observed. An 1895 US Army Corps of Engineers map of the Upper Willamette River, with detailed depictions of buildings and structure along the river shore, does not show any structures at the location of the recorded features of Site 17-98-1. An historic period photograph depicting a river boat docked at Butteville Landing, dated 1890-1895, shows smaller scale docks and pilings, but nothing matching the size and scale of the extant recorded features (see Figure 11). A large structure, at water's edge, first appears in the photographic record in 1905 (see Figure 12). Elements of this structure, and the structure shown on a 1910 photograph (see Figure 13) appear to match up with some features of the concrete structural remains documented on this form, indicating that these features may represent the remains of structures first erected sometime between 1895 and 1905.

#### Site Condition:

The site is in poor condition. The concrete structural remains are exposed to seasonal inundation and river erosion and are actively collapsing.

Rock art? None

Site condition	
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Site condition
Visit date September 25, 2017
Site condition poor
Recorder Matt Goodwin

Artifacts collected? No	
Work performed site recordation	
Protective measures recommended None	
Impacts/impact agents erosion, recreational use	

#### Bibliographic Information:

Corning, Howard M.

1973 Willamette Landings, Ghosts Towns of the River. 2nd ed. Oregon Historical Society Portland, Oregon.

Franklin, Jerry F. and C.T. Dyrness

1988 Natural Vegetation of Oregon and Washington. Oregon State University Press, Corvallis.

General Land Office (GLO)

1851 Plat of Township 3 South, Range 1 West, Willamette Meridian. Microfiche on file, USDI Bureau of Land Management, Oregon State Office, Portland.

McArthur, Lewis A., and Lewis L. McArthur

2003 Oregon Geographic Names. 7th edition. Oregon Historical Society Press, Portland.

Query, Charles F.

2008 History of Oregon Ferries Since 1826. 2nd edition. Maverick Publications, Bend, Oregon.

#### INTERGOVERNMENTAL CONSULTATION FORM



# STATE / FEDERAL AGENCY REVIEW

# A REVIEW OF A PROPOSED OUTDOOR RECREATION PROJECT WHICH FEDERAL ASSISTANCE HAS BEEN REQUESTED.

Project Name: Butteville Landing Restoration Phase 3
Project Sponsor: Friends of Historic Butteville and Marion County
Return Date: June 2019

To Agency Addressed: **This is a Federal Aid Grant. A comment is required**. If your agency cannot respond by the return date, please notify us immediately.

PROGRAM REVIE	W AND COMMENT
We have reviewed the project notice and har relationship to our plans and programs:  [ ] It has no effect. [ ] We have no comment. [ ] Effects, although measurable, would be [ ] It has adverse effects. (Explain in Rem [ ] We are interested, but require more inf (Explain in Remarks section)  [X] Additional comments for project improve	narks section) formation to evaluate the proposal.
REMARKS:	
The site requires a removal/fill from state and fewith the Army Corps of Engineers and DEQ to o	deral agencies. Please continue your coordination obtain your necessary permits.
Reviewed By: Mary Camarata	Title: Project Coordinator
Email address: camarata.mary@deq.state.or.us	Phone: 541-687-7435
Return to: Ben Williams	

Friends of Historic Butteville

# OREGO/V STATE PARKS

## INTERGOVERNMENTAL CONSULTATION FORM

# STATE AGENCY REVIEW

A REVIEW OF A PROPOSED OUTDOOR RECREATION PROJECT FOR WHICH STATE GRANT ASSISTANCE HAS BEEN REQUESTED.

Project Name: Butteville Landing Dock			
Applicant Agency: Friends of Historic Butteville			
	Requested Return Date: May 8, 2019		
ļ	o Agency Addressed: If you intend to comment, but cannot respond by the return date, potify us immediately. If no response is received by the due date, it will be assumed the ave no comment and the file will be closed.  STATE AGENCY REVIEW AND COMMENT		
>	We have reviewed the project notice and have reached the following conclusions elationship to our plans and programs:  It has no effect.  We have no comment.  Effects, although measurable, would be acceptable.  It has adverse effects. (Explain in Remarks Section.)  We are interested, but require more information to evaluate the proposal. (Explain in Remarks Section.)  Additional comments for project improvement. (Attach if necessary).	on its	
=	REVIEW AGENCY REMARKS: Follow the conditions and best management practices per DSL Permit No. 61011, includitions and permit No. 61011, includitions are suppropriate timing for in-water work. If the project will be modified, please contact the local constrict Fish Biologist, Tom Murtagh at 971-673-6044.	ing the ODFW	
Δ	Agency: Oregon Department of Fish and Wildlife		
_	Reviewed By:Joy Vaughan Title: _Land Use and Waterway Alterations Coordinate	or	
_	Email address: _joy.r.vaughan@state.or.us Phone:_503-947-6089	,	

Return to: Ben Williams, Friends of Historic Butteville

# INTERGOVERNMENTAL CONSULTATION FORM



# STATE / FEDERAL AGENCY REVIEW

A REVIEW OF A PROPOSED OUTDOOR RECREATION PROJECT WHICH FEDERAL ASSISTANCE HAS BEEN REQUESTED.

Project Name: BUTTEVILLE LANDING RESTORATION
Project Sponsor: FRIENDS OF HISTORIC BUTTEVILLE
Return Date:
To Agency Addressed: This is a Federal Aid Grant. A comment is required. If your agency cannot respond by the return date, please notify us immediately.  PROGRAM REVIEW AND COMMENT
We have reviewed the project notice and have reached the following conclusions on its relationship to our plans and programs:  [ ] It has no effect. [ ] We have no comment. [ ] Effects, although measurable, would be acceptable. [ ] It has adverse effects. (Explain in Remarks section) [ ] We are interested, but require more information to evaluate the proposal. (Explain in Remarks section) [ X ] Additional comments for project improvement. (Attach if necessary).  REMARKS:
See attached
Agency: State Marine Board
Reviewed By: <u>Janine Belleque</u> Title: <u>Boating Facilities Program Manager</u>

**Return to**: Ben Williams, Friends of Historic Butteville <u>buttevillefriends@gmail.com</u>

503,568.5670

The Friends of Butteville Landing have been in discussion with us since November 2017 about developing public access at this location. Throughout the discussions they have been very receptive and responsive to our comments, questions and concerns.

The Butteville Landing paddle access facility is located in the Willamette River within the 28 mile section of the river known as "Newberg Pool" from the confluence with the Yamhill River to Willamette Falis. The Marine Board comments are made in part based on a comprehensive review of the boating facilities, boating activities, and waterway rules within the Newberg Pool. Additionally, our comments will focus on the proposed Butteville Landing recreational boating facility.

In the Newberg Pool there are seven active public facilities with 9 boat ramp lanes, 352 vehicle/boat trailer parking spaces, 110 single car parking spaces, 1024 linear feet of short term tie up docks and 108 seasonal/annual moorage slips. There are also several private floating structures including four home development dock leases with 109 annual moorage slips and 345 residential docks as of February 2019.

According to the 2017 Triennial Survey of Boaters, there are more than 80,000 boat use days in the Newberg Pool. Boating activities in the Newberg Pool include angling, cruising, paddling, and watersports such as waterskiing, tubing, wake boarding and wake surfing. Watersports is the most popular activity followed by cruising which collectively accounts for 78% of all boating activity in the pool. The peak boating season is July-September with approximately 53% of all boating activity occurring. April-June is also a popular shoulder season with 36% of the boating activities. Nearly 90% of all boating activities occur during a six month period. Additionally, the number of floating structures within the Newberg Pool has more than doubled since 1997.

In January 2019 the Marine Board's governing Board approved new boating operation rules for the Newberg Pool. Butteville Landing is located in an area that allows wakeboarding, waterskiing, tubing, angling and paddling. The facility is in a wake surfing restricted zone.

The proposed dock design extends slightly beyond the line of other adjacent floating structures. This may expose the dock to additional loading factors such as debris, wave, wake, wind, current, and impact. The facility should be designed to withstand environmental and human caused loading for this section of the Willamette River.

It is my understanding that the Oregon Dept. of State Lands permit has been issued but the U.S. Army Corps of Engineers permit is pending. If the dock size or location were to change during regulatory review for any reason, including as a result of ESA minimization or avoidance efforts, then the revised dock location or design would require further evaluation by the Marine Board to determine any possible harmful effects on public use, safety and navigation on the river.



December 4, 2020

Re: Floodplain Development/Greenway Permit Case No. 20-003

**Butteville Landing - Usage and Impact Assessment** 

**Applicant**: Friends of Historic Butteville PO Box 506, Donald, OR 97020

## II. Garbage Pickup and Trash at Butteville Landing

FOHB picks up garbage from the Landing's two garbage cans on Monday morning. Loose refuse or garbage (paper cups, candy wrappers) have been extremely rare, and during 2020 the two gargabe cans have never both been full after a week's time. Volumes of garbage at a property with public access can serve as an indirect indicator of people using the site.

#### June 22, 2020 - [Previously submitted in Hearings Officer written testimony]

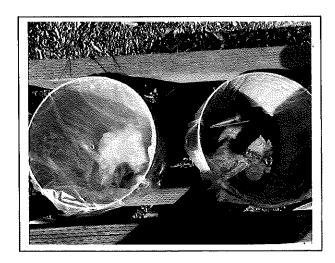
On Monday June 22, 2020 after a full week and following Father's Day Weekend that saw a very large turn out of visitors to Champoeg State Park, both garbage can liners at the Butteville Landing were only half full. See photo below.



There was no litter or loose trash to be found in the Landing. Trash or garbage that blows in by the wind or is carried in by the flow of the river are beyond the control of FOHB, but are picked up during FOHB's regular trash cleanup visits. Correspondingly, visits by FOHB Board members confirmed no people at the Landing the night of Saturday, June 20.

## July 4th Weekend - [Previously submitted in Hearings Officer written testimony]

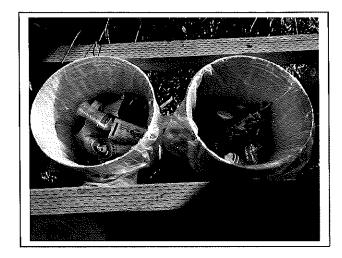
Garbage at the Landing on the morning of July 6 confirms very low usage of the site by the public in the form of two partially filled garbage can liners that consolidated into less than one full liner.





# July 12th Weekend - [Previously submitted in Hearings Officer written testimony]

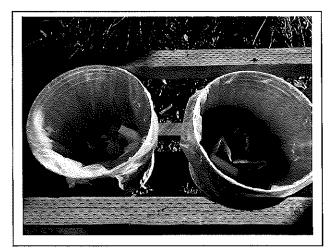
Garbage at the Landing the morning of July 13, again with again with two half full garbage can liners that consolidated into a single liner.





<u>July 19<sup>th</sup> Weekend - [Previously submitted in Hearings Officer written testimony]</u>

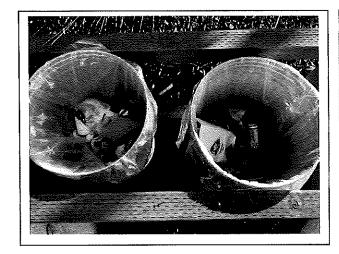
Garbage at the Landing the morning of July 20 confirms low public usage,

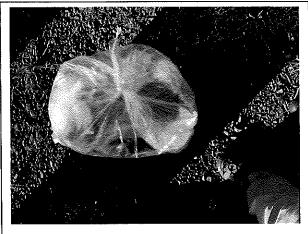




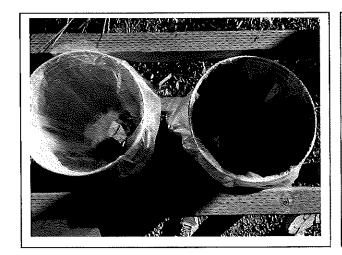
# Garbage Pickup - July 26

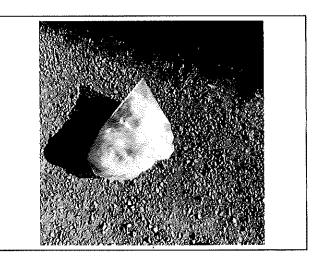
Two partially full trash liners that consolidate into a single liner less than half full.





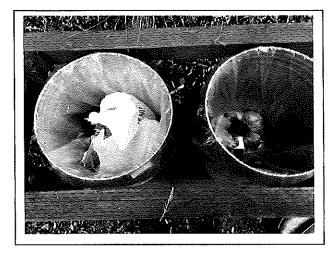
# Garbage Pickup - August 3

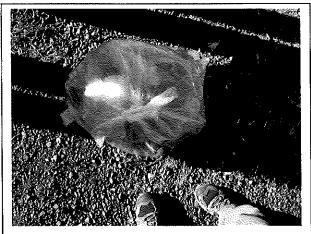




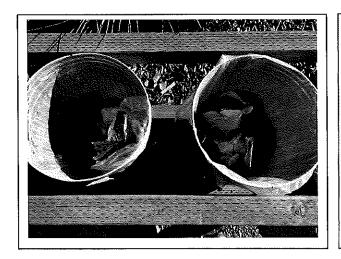
# Garbage Pickup - August 10

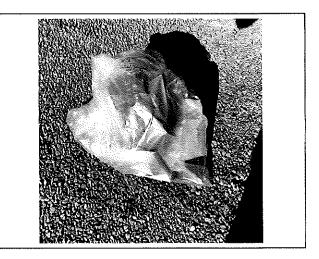
Two partially full trash liners that consolidate into a single liner less than half full.





# Garbage Pickup - August 17

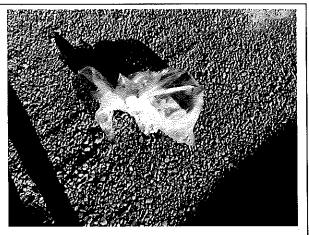




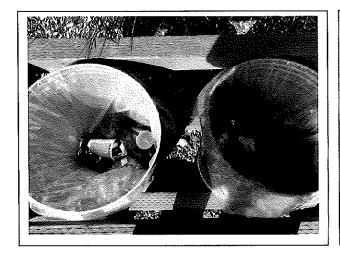
# Garbage Pickup - August 24

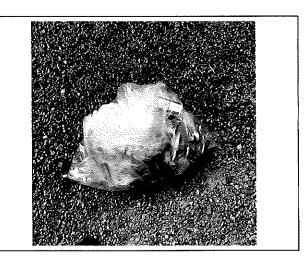
Two partially full trash liners that consolidate into a single liner less than half full.





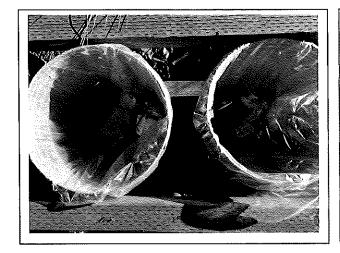
# Garbage Pickup - August 31





# **Garbage Pickup - September 7**

Two partially full trash liners that consolidate into a single liner less than half full.





# Garbage Pickup – September 14

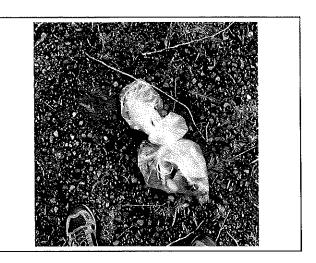




# **Garbage Pickup -September 21**

Two partially full trash liners that consolidate into a single liner less than half full.





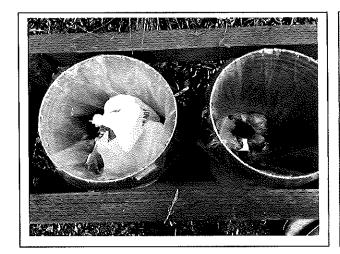
# Garbage Pickup – September 28





# **Garbage Pickup – October 5**

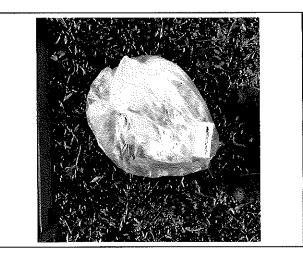
Two partially full trash liners that consolidate into a single liner less than half full.





# **Garbage Pickup – October 12**





## Garbage Pickup – October 19

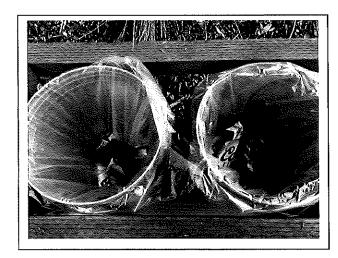
Two partially full trash liners that consolidate into a single liner less than half full.





#### **Garbage Pickup - October 26**

Two partially full trash liners that consolidate into a single liner less than half full.

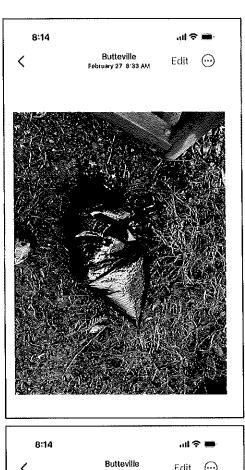


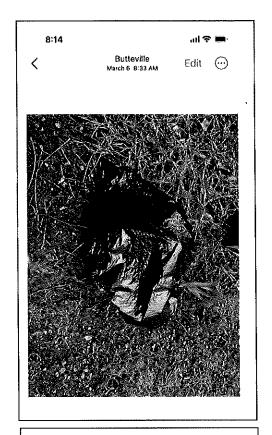


The weekly accumulated garbage demonstrates that the Historic Butteville Landing is a low use and low impact site.

It further supports the assertion made in written testimony during the initial Floodplain appeal, that the public disturbance and so-called criminal activity reported by the Appellants and able to be substantiated by the County Sheriff's Office, was a one-time event tied to general closure of State and County Parks, leaving the Butteville Landing one of the very few venues still open to the public.

# **BUTTEVILLE LANDING - WEEKLY GARBAGE COLLECTION DOCUMENTATION 2023**

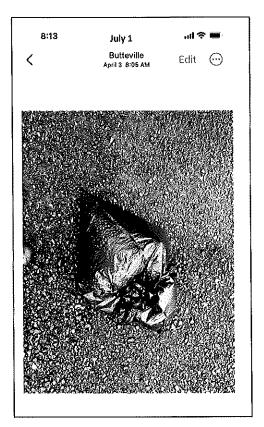


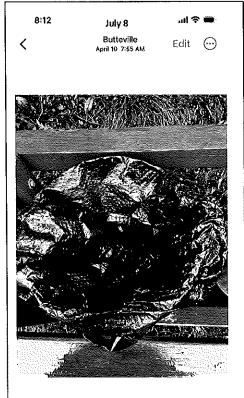




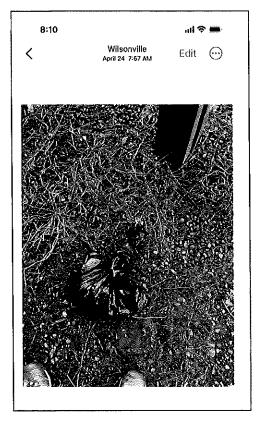




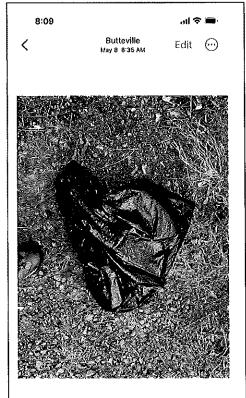




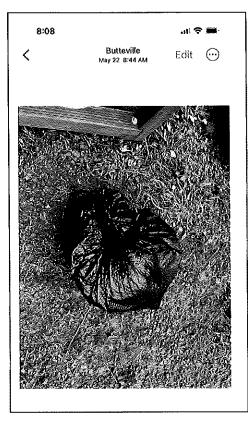




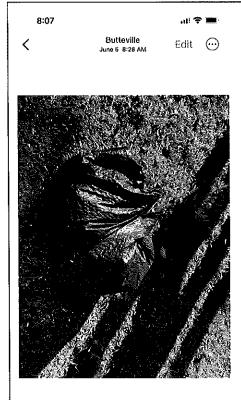


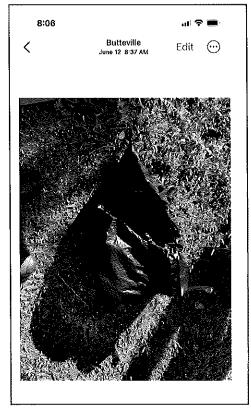




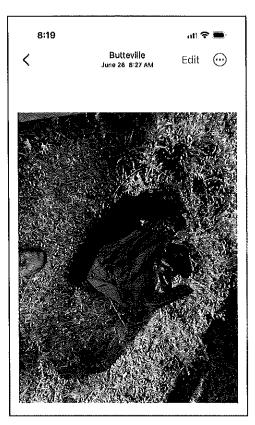




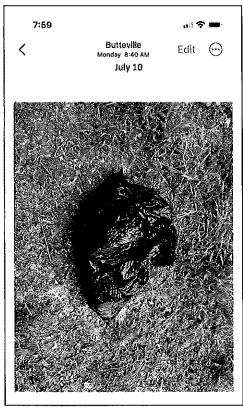


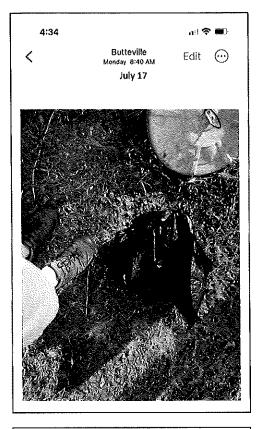


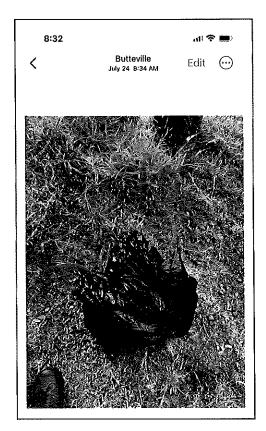


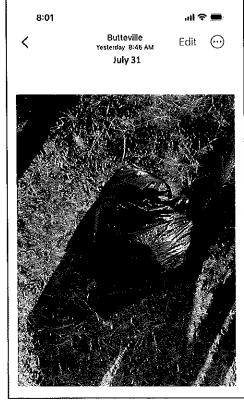


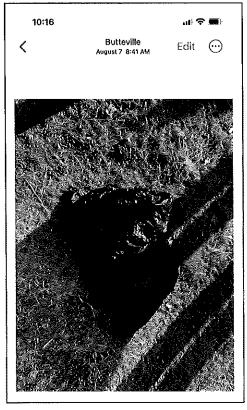




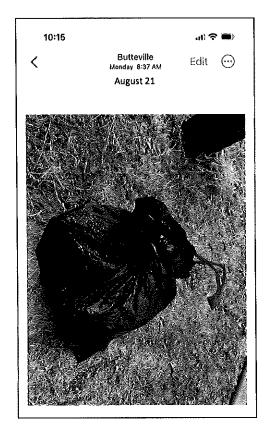


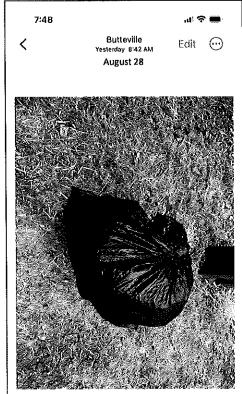


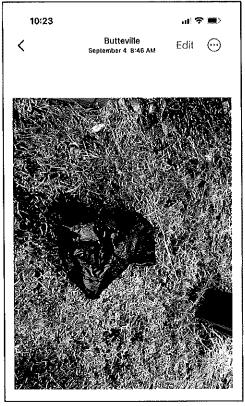


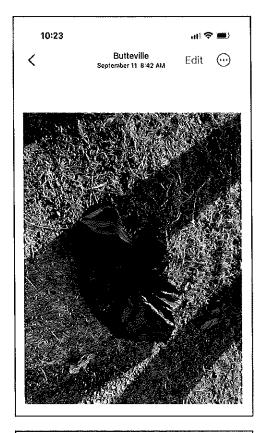


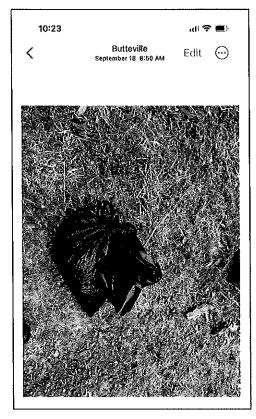




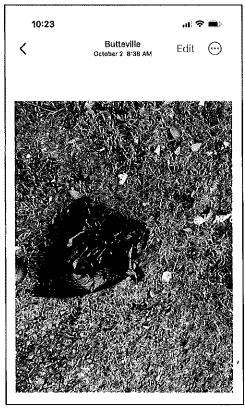


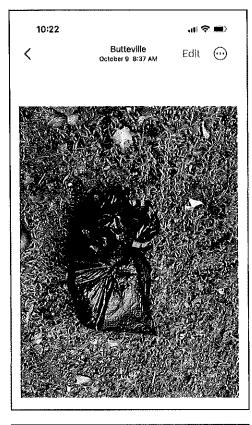


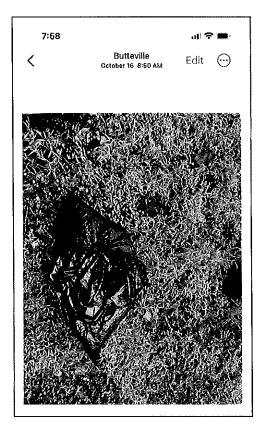


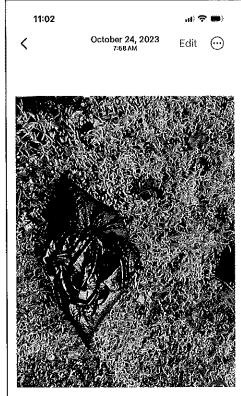


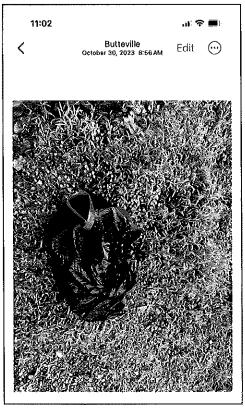


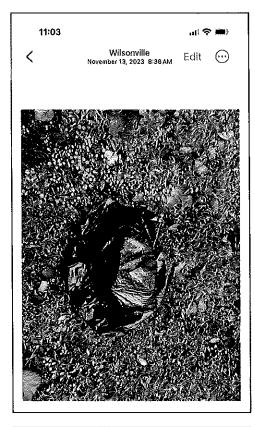




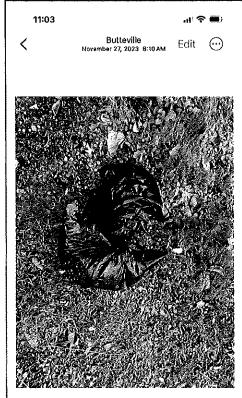


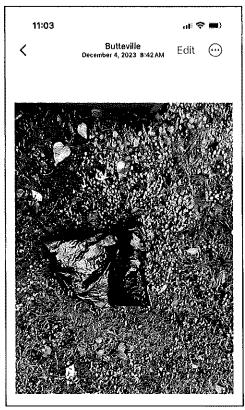


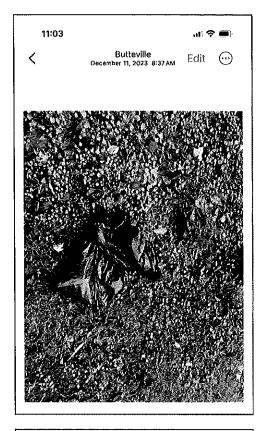


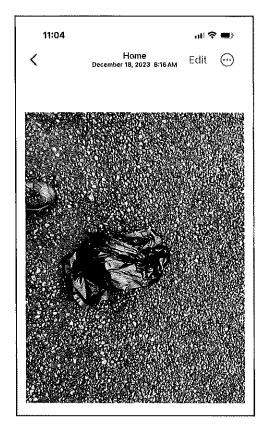


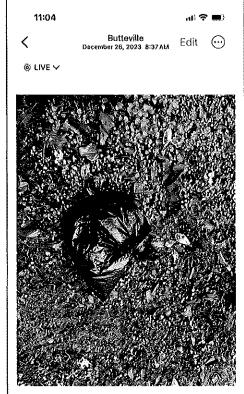


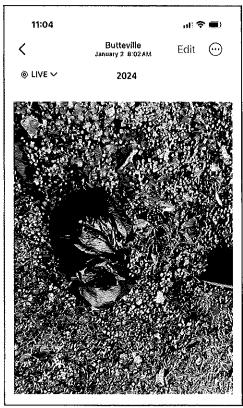












December 13, 2021



### Boatwright Engineering Inc.

2613 12th ST SE, SALEM, OREGON 97302 civil engineers • land surveyors

503 363-9225 FAX 363-1051

Brandon Reich Marion County Planning Dept. 5155 Silverton Road, NE Salem, Oregon 97301

FLOODPLAIN DEVELOPMENT/GREENWAY PERMIT APPLICATION

Dock & Gangway, Butteville Landing Butte Street Public Right-of-Way Willamette River Mile 42.93

#### Dear Brandon,

Re:

Following, you will find responses to items that I anticipate will be required by conditions applied to a favorable decision on the above referenced permit application. These items pertain to the construction work that would be involved at the site. This work requires certification by a registered professional engineer.

#### 17.178.050 Conditional use procedures and requirements.

D. Prior to obtaining a building permit, commencing development or placing fill in the floodplain the applicant shall submit a certification from a registered civil engineer demonstrating that a development or fill will not result in an increase in floodplain area on other properties and will not result in an increase in erosive velocity of the stream that may cause channel scouring or reduce slope stability downstream of the development or fill.

I used HEC-RAS version 6.1.0 to model the comparison between the existing flood elevation and velocity and the resultant flood elevation and velocity that will exist once the proposed improvements are constructed.

This site is located on the right bank of the Willamette River in north Marion County. To evaluate the location, I had to determine the base flood elevation and the river flow velocity at river mile 42.93 which is the most upstream point on the proposed dock installation. I obtained LIDAR bare earth topography from the Oregon Department of Geology and Mineral Industries (DOGAMI) encompassing both banks of the river from river mile 42.66 to 43.30. I also utilized the cross-section provided by Flowing Solutions on Sheet 6 of their Butteville Landing River Access plans, dated 5/8/19. All of this data is on NAVD88 datum which I then converted to NGVD29 to match the standard currently used by Marion County and FEMA.

I did not have any data source for the shape for the Willamette River bottom. I set the bottom elevations at cross-sections C, D and E, per page 108P of the Flood Insurance Study (FIS) for Marion

County (FIS No. 41047CV003B), dated October 18, 2019. I then looked at the floodway data for the Willamette River and used the Floodway Width, Floodway Elevation, Floodway Water Surface, and, the Floodway Cross-Sectional Area from Table 6 in Volume 1 of the FIS study noted above. Using trial and error calculations of the shape of the river bottom, I derived the configuration that matched all of the parameters of the Floodway Data in said Table 6, with the exception of the Floodway Mean Velocity. My velocities at the C, D, and E cross-sections were slightly faster. See my Calculations Chart, attached. The only way to slow the velocity down to meet the FIS numbers would be to enlarge the cross-sectional area, or change the bank coefficient, which would increase the height of the base flood elevation. I chose to leave the velocity at the rate I calculated.

I then checked the 10, 50, and 100-year flood elevations for the associated cross-sections and compared those to the flood profile (page 108P referred to above). When doing this, all elevations matched FEMA's levels. This gave me the 100-year BFE at river mile 42.93.

The ninety-degree angle of the cross sections, relative to the water flow, finds that the pilings are not in alignment. They are slightly off, so that the two tallest pilings, located at the north and south ends of the improvement, and which extend the furthest into the river, are not in line with any other pilings or components. Some of the shorter pilings, located between the tall end pilings, fall in paired alignment with the concrete pad/abutment. Other intermediate pilings do not line up with each other, or anything else, perpendicular to the line of flow. These last two scenarios have a much smaller effect on the water level than that which the end pilings cause. I did not include the flotation components since they will rise with the water level. I also evaluated the six trees that were recently removed at the site, which totaled 8.25 feet of width. I found that they were not in the same cross-section as the piling placements and could not be included in the study area, but would have had some impact on the river flow.

The cross-sectional area impacted by the pilings at the south end of the project produces a 0.02-foot increase in vertical elevation of the floodplain surface. This is below the 0.1-foot threshold that FEMA can monitor. To address the 0.02-foot rise, I looked at FEMA's Conveyance Compensation Analysis which involves removing some material from the same cross section wherein the partial obstruction from the pilings is located. In this case, excavation will compensate for the pilings and related improvements to ensure that there is no net rise in the river level at the base flood stage.

Because the tall pilings have the greater impact, their heights and locations establish the end area of the proposed compensatory excavation. The Conveyance Compensation Analysis calculations demonstrate that excavation of a 20.0 square foot cross sectional area on the upstream end and a 41.5 square foot cross sectional area on the downstream end will ensure no net rise during a flood. The proposed excavation across the entire south-to-north length of the dock improvement area will transition between 20.0 square feet on the south to 41.5 square feet on the north. This will fully compensate for the impact of the pilings and the concrete dock support being placed. The excavation will total 41.1 cubic yards, removed to an off-site location, which will meet the FEMA conveyance calculation requirement for no rise.

The intermediate pilings are shorter in height and the calculations show that no compensating excavation is needed for these.

I certify that the installation of the proposed pilings and the soil removal based on the Conveyance Compensation Analysis will not produce an increase in floodplain area on other properties.

Using the US Army Corps of Engineers' Rule of Thumb for Scour at Vertical Piles for Small Diameter Piles and the Corps' Scour at Vertical Piles, Scour by Currents-Small Diameter Piles formula, the limits of potential scouring for the piles at this site, that are located in the main channel, could be 2.0 to 3.5 feet in depth and could extend out from the piling at a 1:1 slope for a maximum radius about the piling of 2.5 to 4.0 feet. The two piles outside of the main channel, where the flow velocity is less than 2.5 ft/sec, will not produce any scouring.

I certify that this development may cause localized scouring but will not produce channel scouring and will not reduce slope stability downstream of the development site. The area where the soil has been removed should resist scouring provided the ground cover has been reestablished.

#### 17.178.060 Flood protection standards.

In all areas of identified floodplain (which includes all areas of special flood hazard), the following requirements apply:

- J. Floodways. Located within areas of floodplain established in MCC 17.178.030 are areas designated as floodways. Since the floodway is an extremely hazardous area due to the velocity of floodwaters which carry debris, potential projectiles and erosion potential the following provisions shall apply in addition to the requirement in subsection (I) of this section:
  - 1. Prohibit encroachments, including fill, new construction, substantial improvements and other development within the adopted regulatory floodway unless certification by a registered professional civil engineer is provided demonstrating through hydrologic and hydraulic analyses performed in accordance with standard engineering practice that the proposed encroachment shall not result in any increase in flood levels within the community during the occurrence of the base flood discharge.
  - 2. If subsection (J)(1) of this section is satisfied all new construction and substantial improvements shall comply with all applicable flood hazard reduction provisions of this section.
  - 3. The area below the lowest floor shall remain open and unenclosed to allow the unrestricted flow of floodwaters beneath the structure.

Based on my HEC-RAS 6.1.0 modeling of this reach of the Willamette River for the encroachment of the gangway, dock, and related structures and supports, I can certify that this construction will not result in any increase in flood level during the occurrence of the base flood discharge. If you require additional data from my HEC-RAS analysis, please let me know.

The proposed dock and gangplank will float on the water, and the flow of floodwaters will not be restricted beneath these structures. The proposed concrete abutment at the east end of the gangplank is not within the floodway.

The information provided in response to 17.178.050 D., above, for the cross-sectional area impacted by the pilings, along with the Conveyance Compensation Analysis, demonstrates that no net rise shall

occur due to this construction.

I certify that the installation of the proposed pilings will not produce an increase in flood levels within the community during the occurrence of the base flood discharge.

The compensatory removal should be done after the winter rains and when the river level is below the work area. All of the existing riprap in the removal area should be set aside and replaced in the same area from which it came. A silt fence must be installed prior to any work commencing and maintained until grass seed has developed to a fully protective groundcover.

The Cross Section shown on Sheet 3 of 3 is at the south tall pier and does not reflect the cross section where the concrete abutment is located. The concrete abutment shown on this section view is downstream and is only included to portray the location within the typical river cross section.

Any issues that arise from Marion County Code MCC 17.178.060(C), (D)(1), (E), (F) are addressed per the letter dated 29 May 2020 from Kelly D. LaFave, PE.

Please contact me if you have any questions.

Sincerely,

Corbey Boatwright, PE

Corby Breaking (1)

Renewal Date: December 31, 2021

Attachments:

Copy of letter from LaFave to Reich, 29 May 2020

FEMA FIRMette

FIS, Marion County, Table 4, Table 6, & Page 108P

**HEC-RAS** Butteville Dock cross-sections

HEC-RAS 5.0.1 Output Results HEC-RAS Pre-Dock Output HEC-RAS Post-Dock Output Engineering Plans (3 sheets) Conveyance Calculations

CC: Ben Williams, president, Friends of Historic Butteville



# MARINE STRUCTURES ENGINEERING, INC.

1004 Commercial Avenue, #364 Anacortes, WA 98221 (360) 466-8627 Fax: (360) 230-2310

29 May 2020

Mr. Brandon Reich Marion Planning Department 5155 Silverton Road NE Salem, Oregon 97301

RE: Floodplain Development/Greenway Permit Case No. 20-003 Dock and Gangway, Butteville Landing Butte Street Public Right-of-Way Willamette River Mile 42.93

Dear Brandon:

Based on the review of the pile supports and gangway plans prepared by me and review of the float plans prepared by others,

I certify that the conditions applicable to pile supported, floating dock and walkway structures of Marion County Code Chapter 17.178, Floodplain Overlay Zone, specifically subchapter 17.178.60 Flood Protection Standards, sections (C), (D1), (E) and (F) will be met by the proposed design.

It is my understanding based on review of the project drawings and discussions with the contractor, that there will be at least twenty (20) feet of clearance between the proposed float and the existing nearest downstream float.

Please let me know if you have any questions or need any additional information.

Sincerely,

MARINE STRUCTURES ENGINEERING, INC.

Kelly D. LaFave, P.E.

President

SUL 31 DEC ZULU

PURPLE WALK FROM THIS PHOTO

Par

GREEN FROM PLANS

> USED CONCRETE TO LINE UP DOCK

Google Earth

# National Flood Hazard Layer FIRMette

122°50'66 86'W



OTHER AREAS OF FLOOD HAZARD OTHER AREAS 12<u>2°50'19.41"W</u> MINIMAL DSGS The National Way. 1:6,000 EDIAREA 1,500 **COUNTY UNINCORPORAT** 2 SKINIVS) 250 45°15'57 54"N

# **Legend**

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

With BFE or Depth 2000 AE AG, AH, NE, AR Without Base Flood Elevation (BFE) Regulatory Floodway SPECIAL FLOOD HAZARD AREAS

depth less than one foot or with drainage areas of less than one square mile zons x of 1% annual chance flood with average Future Conditions 1% Annual

0.2% Annual Chance Flood Hazard, Area:

Area with Reduced Flood Risk due to Chance Flood Hazard Zone x Levee. See Notes. Zono x

Area with Flood Risk due to Leves 2000 D No screen Area of Minimal Flood Hazard Zene x

**Effective LOMRs** 

Area of Undetermined Flood Hazard Zone

Channel, Culvert, or Storm Sewer GENERAL

STRUCTURES | 1111111 Levee, Dike, or Floodwall

(B) 20.2 Cross Sections with 1% Annual Chance Water Surface Elevation

---- Base Flood Elevation Line (BFE) Coastal Transect

 Jurisdiction Boundary - Umit of Study

Coastal Transect Baseline

Hydrographic Feature Profile Baseline

OTHER FEATURES

No Digital Data Available Digital Data Available

Unmapped

MAP PANELS

The pin displayed on the map is an approximate point selected by the user and does not represen an authoritative property location.

This map compiles with FEMA's standards for the use a digital flood maps if it is not void as described below. The basemap shown compiles with FEMA's basemap accuracy standards

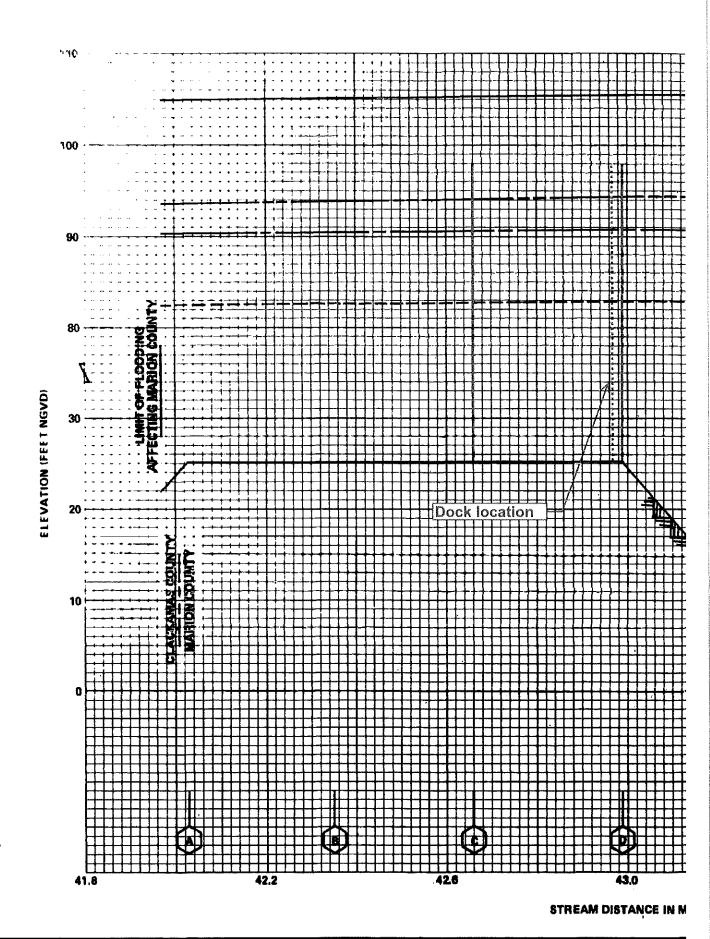
authoritative NFHL web services provided by FEMA. This map was exported on 4/2/2020 at 6/0027 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or The flood hazard information is derived directly from the become superseded by new data over time. This map image is void if the one or more of the following map FIRM panel number, and FIRM effective date. Map images for legend, scale bar, map creation date, community identifiers, unmapped and unmodernized areas cannot be used for regulatory purposes.

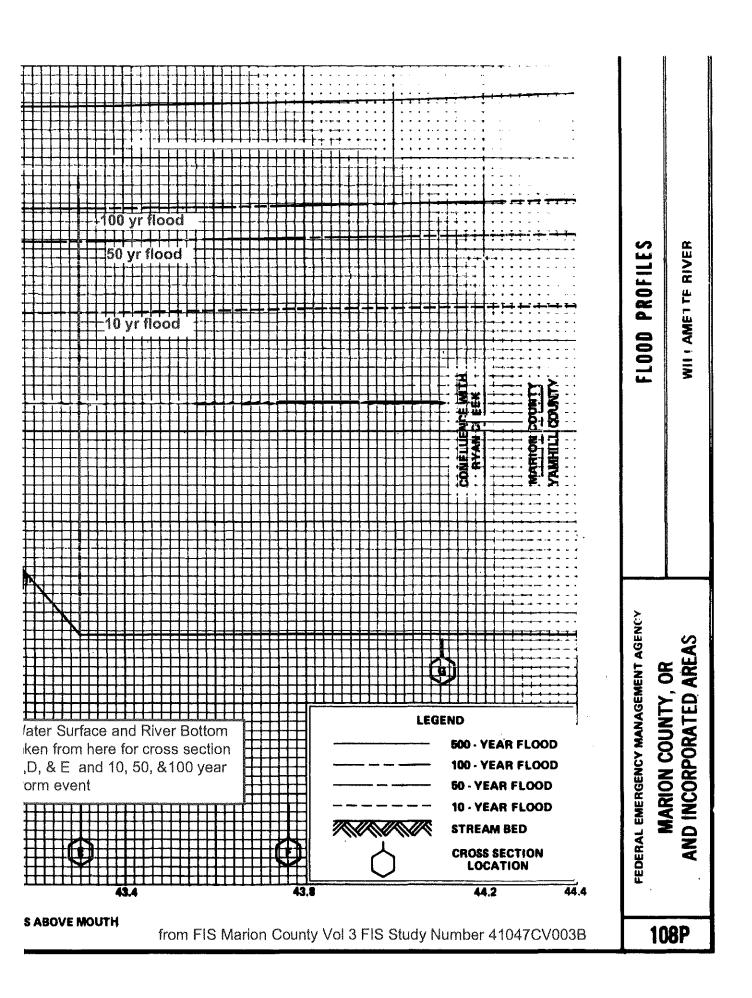
Table 4. Summary of Discharges (Cont'd)

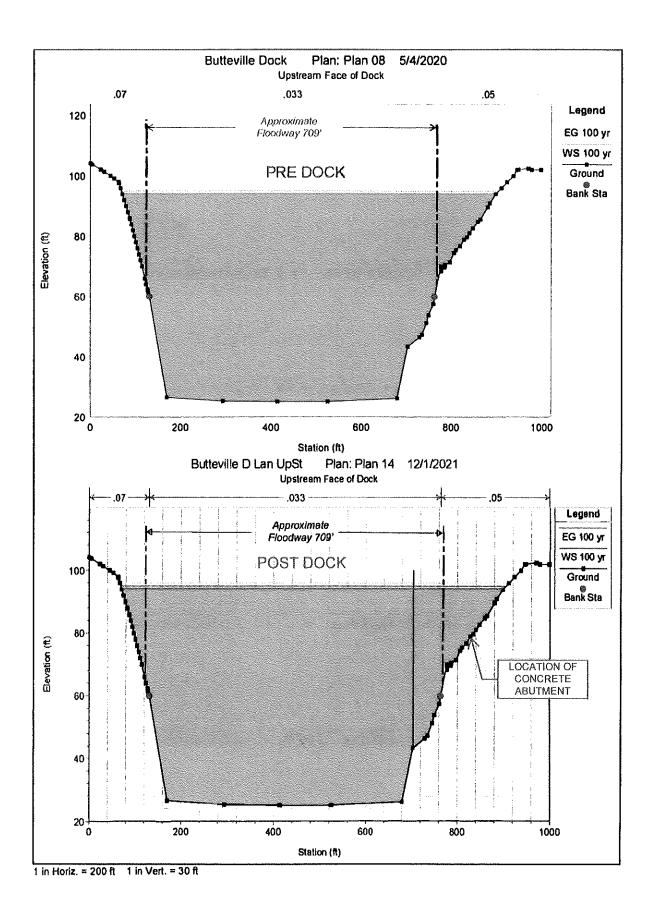
Flooding Source and Location	Drainage Area (Square Miles)	Peak <u>10-Year</u>	Discharges (C 50-Year	Peak Discharges (Cubic Feet per Second)  at 50-Year 100-Year 50	cond) 500-Year
West Fork Pringle Creek At mouth	3.2	5005	650²	730²	880²
Approximately 450 feet downstream of flood control structure	3.1	460	290	999	800
Just downstream of Pringle Road	2.6	400	515	280	695
Just upstream of Commercial Street (Highway 99E)	1.9	325	420	470	565
Willamette River			A PART OF THE PART	S. T. T. S.	
At Butteville	8,380	182,000	260,000	302,000	445,000
At Salem	7,280	190,000	250,000	280,000	363,000

<sup>1</sup>Data not determined <sup>2</sup>Urbanized runoff from Pringle Creek basin

FLOODING SOURCE	SOURCE		FLOODWAY			BASE FLOOD WATER-SURFACE ELEVATION	LOOD SE ELEVATION	
CROSS SECTION	DISTANCE1	WIDTH <sup>2</sup> (FEET)	SECTION AREA (SQUARE FEET)	MEAN VELOCITY (FEET PER SECOND)	REGULATORY	WITHOUT FLOODWAY (FEET	JT WITH AY FLOODWAY (FEET NGVD)	INCREASE
Willamette River A	42.03	710/370	43,332	9.9	93.7	93.7	94.6	0.9
	42.66 42.66 42.99	700/385	43,336 43,605	6.6	94.1	94.1 84.3	94.9	0.8
J	43.30	680/381	39,287	7.4	94.4	94.4	95.2	0.8
ים ד	43.76	700/415	40,368	7.1	95.0	95.0	95.9	0.0
<b>I</b>	4. 8 8. 4.	750/430 2,100/1,690	41,438 47,272	6.9	95.3 96.2	95.3 96.2	96.0	0.7
<b>-</b> ×	47.64	3,000/2,525	56,285 46.825	5.1	97.5 97.5	97.5 97.5	98.1	0.6
; <u>.</u> ;	48.46	3,000/2,550	47,512	6.0	97.5	97.5	98.4	6.0
∑ Z	50.65	8 000/7 380	77,593	3.7	98.5 99.3	. 88 53.53	100.1	0.8 0.8
: 0	51.59	8,000/6,050	129,683	2.2	99.5	99.5	100.4	6.0
۵. (	52.48	7,700/7,375	82,487	3.5	99.5	99.5	180.4	0.0
> ∝	54.17	5,380/2,260	18,889	2.5	101.4	101.4	102.3	6:0
S	55.17	4,500/625	74,363	3.4	101.4	101.4	102.3	6.0
L ;	55.71	4,100/840	76,317	3.3	8.101	101.8	102.6	8.0
<b>&gt;</b> :	56.4 4.0	3,600/3,240	88,098	5.6	102.2	7.701	105.0	, C
> 3	57.55	7,000/6,760 8,000/7,755	144,46/ 210,016	8.I 7.	0.70T	102.9	103.8	0.0
: ×	59.06	7,400/7,100	172,084	1.5	102.9	102.9	103.8	0.9
7 ×	59.42	7,800/7,260	199,965	1.3	103.3	103.3	7 1. 4. 1. 4.	O O 8. 80
				from FIS M	from FIS Marion County Vol 2	<u> </u>	Study Number 41047CV002B	47CV002B
'Miles above mouth 'Tote	Total width/width within Marion County	rion County	***************************************		***************************************			
	FEDERAL EMERGENCY MANAGEMEI	ICY MANAGEMENT	VT AGENCY		FLO	FLOODWAY I	DATA	
-i ш - с	MARION COUNTY, AND INCORPORATED	OA	JR IREAS		MILI	WILLAMETTE RIVER	IVER	







#### rev. 12-01-2021 HEC-RAS 5.0.1 OUTPUT RESULTS

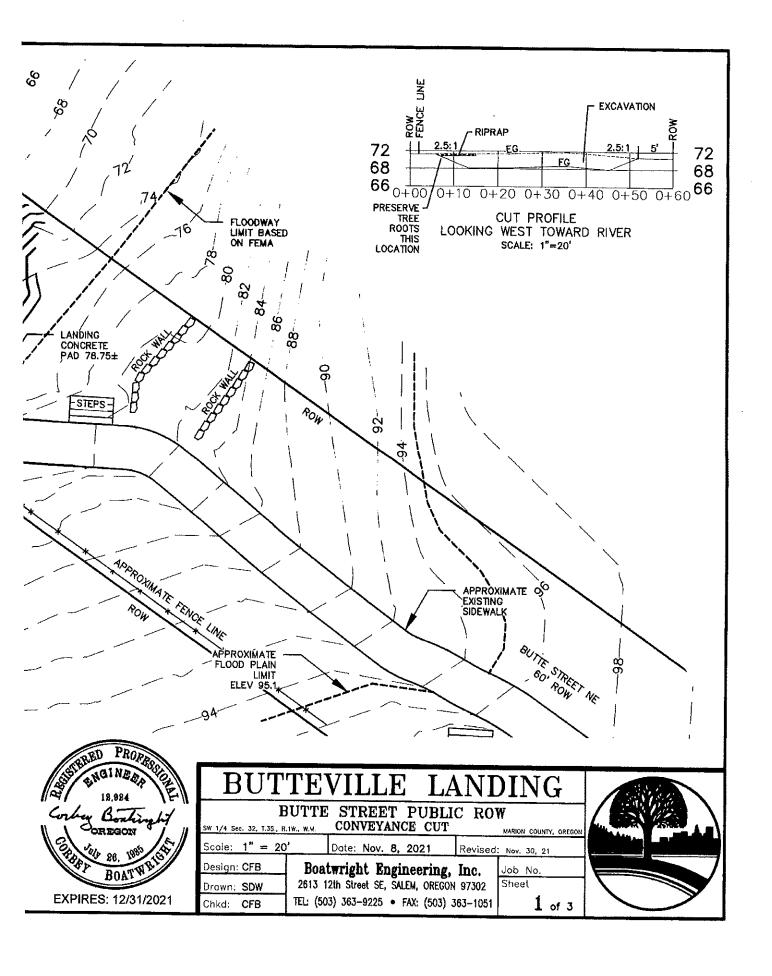
Dock & Gangway, Butteville Landing Butte Street Public Right-of-Way Willamette River Mile 42.93

Match Information FIS Vol 1 of 3 Marion County FLoodway Data Williamette RiverTable 6

	HEC DAR	Dani Basi		Dume it.		aO Daambi D	hada-la Ded	14 155	••••							
		River		Profi			Suttente Prof		C# UI C	E O 51	5.0 Mana	Vel Clark	Floridania I	T 111-4		14-1 Block
	Reach	LUYER	- DIE	Fluci	·	O Your		W 8. Elev	Cri W.B	E G Elev	E.G. Slope	100	Flow Area	Too YHOO		Val Right
e	B. Haudin	1.00			[	(6/3)	(ñ) ·	(fi) .	(h)	(ft)	(A/R)	(IV)	(Iq ft)	(10)	(8/4)	(IVa)
	Butterife	43,30		100 <u>yr</u>		302000 00	7.50	95 17		23 11	0.000135	7 78	39287 18	680 00	7 69	128
Đ	Butteville	42.99		100 yr	11.0	302000.00	25 20	95,07		95.67	0.000101	7 28	43805 06	709 00	6 93	2 11
	Butteville	42,03		100 yr	5	302000 00	25 10	95 05		95 84	0 000100	7 18	43556 15	707 40	6.93	1 83
G	Butteville	42.60	- 1	100 yr		302000 00	25 10	94 90	47 66	95 70	0.000100	7 19	43335 82	700 00	0.97	1 83
	FIS Vol 3	of 3 Mar	lon C	ounty I	nform	ation from I	Flood Profile	page 108P						SHEER ENG	PROFE	
	Reach	River	Si a I	Profé	•	Q Total	W.S. Elev							100	DD.	
			1			(cfs)	(ft)							ARED	1 KUP	
	Butteville	43 30		10 yr		18200000	63 0							10 kg		10
E	But teying	43.30	1	50 yr	***	260000 00	90.6						- // /	\$\\'\	INEED	11.00
	Bulleville		ļ		- 1			-					// A	8/ W.	~~?	151
	DOING A min	43.30		100 yr		30200000	94.4						I/ed	7/ 1	2.924	151
					1									٠, ٠		1 - 11
	Bulleville	42 99		10 yr		182000 00	82 9			Alla	elevation		$\boldsymbol{C}$	m lane i	R-T	14
D	Butteville	42.99		50 yr		260000 00	90.9								and the state of the second	er 1
	Butteville	42.99		100 yr	. å	302000 00	94 3			INGVD	29 Dati	ım l	- 1/	\ \topic	EGON	• / //
												••••	<b>\</b> \	3/ ′	_	15-11
	Bulleville	42.93		10 yr		182000 00							110	300 100	~ 108b	/.9//
	Butteville	42.93	. ]	50 yr	į	260000 00							1	AN TO	28, 19	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
	Butteville	42.93	- )	100 yr	į	302000 00							`	ADE V	War and	<b>~</b> //
		7	1												86, 1985 BOATW	
	Butteville	42 66		10 yr		182000 00	62 8									
C	Butteville	4266		50 yr	7	260000 00	907						REI	NEWAL C	ATE: 12/3	1/2021
	Butteville	42 66		100 yr	•	302000 00	94.1						NL.	ACAAVE C	MIL. 12/0	112021
						*********	•••									
				_				L	Pre Doi	ck						
	HEC-RAS					elle R Reach										
	Reach	Riyer	SI4	Profil	•	O Total		WS Elev		E.G. Eley	E.G. Slope	Vel Chni	Flow Area	a samula of the contraction of		Vel Right
						(CI 1)	(10)	(ft) }	(51)	(ñ)	(fVft)	(ft/s)	(6Q ft) !	(h)	(IVs)	(1/4)
	Butternie	43.30		10 yr		182000 00	7 50	83 00		83 54	0 000 108	5 90	31841 77	750 49	5 75	1 44
能	Butteville	43 30		60 yr_		260000 00	7 50	90 96		9174	0 000128	7 15	3775 9 08	790 70	6 89	1 63
	Butteville	43 30		100 yr		302000 00	7 50	(4 39		95 32	0 000138	7.80	40319-21	694 60	7 43	188
		į	1		i											
	Buttevela	42 99		10 yr		182000 00	25.20	82 92		83.37	0.000073	5 39	35324 46	79121	5 15	1 10
D	Butteville	42.99		50 yr		260000 00	25 20	90 56		91 53	0 000093	665	42034 19	67875	6 19	1 50
	Butleville	42.99		100 yr		302000 00	25.20	94 28		95 09	0.000103	7 28	45088 32	903.52	6 70	176
	.=	7 77			1.1											
	Butteville	42.93	- 1	10 yr	100	162000 00	25 10	82 91		03 34	0.000072	5 32	35198 96	755 90	5 17	1 04
	Butterne	42.93		50 yr		260000 00	25 10	90 84		91 50	0 000092	6 58	4140623	807 24	6.28	
	Buttevstie	42.93				302000 00		(PI 26)		95.05	0.000103				ALCOHOLD STREET, STREE	153
	COLIETAR			100 yr		302000 00	25 10	1920	,	1303	0.000103	(22)	44204.86	820 74	(883)	(1.76)
		4 :: ::	į					***								
_	Bulleville	42.66		10 yr		182000.00	25 10	82 60	41 60	6324	0.000072	5 3 3	35035.79	741 12	5 19	1.17
С	Butterike	42.56		50 yr		260000 00	25 10	90 70	45.71	91 37	0.000092	8.60	41048 49	781 45	6 33	1 60
	Butteville	42 66	i	100 yr		303000 00	25 10	94 10	47 68	94 91	0 000103	7.25	43735.06	800 35	6 91	1 60
								_								
	HEC-RAS	fites Diss	100	O 161	beams 6	eR Reach E	and and a	L Po	ost Dock Up	ostream						
								141 B Ph.	g. 4 (616	F A FI	e e e e	M. Cont.		P		
	Reach	River	0139	Profit	•	Q Yotel		WS Elev	CrtWs	E G Elev	E.G. Slope		FION ATES	Lob Aylosy		Vel Right
			بُ		}	(cfs)	(A)	(称)	(fi)	(A)	(Mg)	(ft/a)	(EQ #)	(ft)	(44)	(ft/s)
	Buttavas	43 30		10 yr		182000 00	7 50	63 01		83.55	0 000108	5 89	31849 12	750 54	5.75	1 44
E	Butteville	43 30		50 yr		260000 00	7 50	<b>©</b> O <b>⊙</b> 7		91 76	0 000126	7 15	37771 12	790 61	6 00	186
	Bulleville	43 30		100 yr		302000 00	50	84 41		95 34	0 000138	7 79	40835 84	895 06	7 43	1.00
		1														
	Butleves	42 99		10 yr	)	182000 00	25 20	82 93		63 38	0.000073	5 39	35332 25	201.42	5.15	3 10
Ð	Bulleville	42.99	į	50 yr		26000000	25 20	80 08		9155	0 000093	8 64	42047 84	578 86	8 10	1.50
	Buttersta	42 99		100 yr	!	30200000	25 20	94 30		95.11	0 000103	7.57	4510323	903 85	0.70	1 76
		1														
	Butteyse	42 93	··j	10 yı		182000 00	25 10	82 91		83 35	0 000084	5.32	3516 5 31	754.95	5 18	1 13
Upstream	Buttaville	42.93		50 yr		260000 00	25 10	90 85		9151	0 000110	6.58	41371 35	608 31	6.28	167
Piling	Butteville	42.03		100 yr	4	30200000	25 10	(94 27)		95.07	0.000124	(721)	44167.65	826 39	(6.84)	(184)
		1	···i	· 7.7. \$1,			10.0	William Commence			~ von 183	San Parison II		220 49	- Comment	184
	Butterste	42 68		10 yr		162000 00	25 10	82 80	41 60	83 24	0.000072	5 33	35035 79	741 12	5 19	5.17
r	Buttersee	42 66				26000000			45.71	91 37						
ų.	Butteville			50 yr			25 10	90 70			0.000092	8 60	41048 49	781 45	6.33	160
	BURTOVIKO	42.66	;	100 yr		302000 00	25 10	94 10	47 66	94 91	0.000103	7.25	43736 08	860 35	6 91	1 60
	HEC DAG	D D	400	D 11	42	on Daniel	3.4011.	Pot	et Dock Dos	enstream						
						e R Reach I				D - D - D						
	Reach	River	<b>∜(8</b>	Prof	<b></b>	O Total	Min Ch El	WS Elev	Cnt W.S	E G Elev	EG Slope į		Flow Area	Top Width		Vel Right
	1					(cfe)	(A)	(n)	(A)	(ft)	(R/A)	(fl/a)	(64 th)	(h)	(R/a)	(Ns)
197	Buttervie	43.30		10 yr		182000 00	7.50	63.01		63.55	0 000108	5 89	31850 95	750 55	5.75	1 44
E	Butteville	43 30		50 yr	]	260000 00	7 50	60.07		9176	6 000126	7 15	37773 59	790 84	6 88	1 66
	Guttersa	43 30		100 yr	) 	302000 00	7.50	94 41		95 34	0 000138	7 79	40839 04	695 14	7.43	1 88
	+															
	Butleville	42 99		10 yr		182000 00	25 70	68.69		83 38	6 000073	5 39	35334 20	791 47	5.45	1 10
Đ	Butterwe	42.99		50 yr	1	260000 00	25 20	90 00		91.55	0.000093	6.84	42050 43	878 68	8 18	1 50
	Buttevale	42.99		100 yr		302 000 00	25 20	94 31		95 11	0.000103	7 27	45 108 47	90388	8 70	178
	. 555555.	<u>.</u> 17 33		15.7. <b>6</b> 7							3 2 100				- 10	
	Butteyste	42.93		10 yr		182000 00	25 10	02.91		63 33	0.000087	5.52	35156 39	754 97	5 18 <sup>1</sup>	1 15
Downstream	Butterse	42 93		50 yr		260000 00	25 10	90.85		91 52	0 000114	8 58	41363 14	808 33	629	1 70
Piling	Buttevide	42.93					25 10	The state of the s		95 07	0 000114	ACCORDING TO THE PARTY OF THE P			AND DESCRIPTION OF THE PERSON NAMED IN	A PROPERTY OF THE PERSON NAMED IN
	threads	74.84		100 yr		302000 00	An 10)	(94 28)		A2 01	0.000129	(721)	44160 11	628 41	(B84)	(101)
	D.Herm	40.00		10		160000 00	25 10	62.64	44.00	0001	0.00000		36005 30	*** **	* **	4.49
c	Buttevite	42 66	- 4	10 yr		162000 00	25 10	82 80	41 60	8324	0.000072	5 33	35035 79	741 12	5 19	1 17
C	,	42 68	į.	50 yı		269000 00	25 10	90 70	45.71	9137	6 000092	880	41048 49	781 45	6 33	160
	Butterne	42 66		100 yr		302000 00	25 10	94 10	47 66	84 91	6 000 103	7 2 5	43736 08	80035	6.01	1 80

100 yr Flood	WS Elev	Velocity Total	Velocity Channel	Velocity Right
Pre Dock	94.26	7,22 ft/s	6.83 ft/s	1,76 ft/s
Post Dock Upstream	94.27	7.21 ft/s	8.64 ft/s	1,94 ft/s
Post Dock Downstream	94.28	7,21 ft/s	8.84 m/s	1 97 9/4

BUTTEVILLE DOCK BARE EARTH 5-1-20.DWG



#### Pre-Dock

HEC-RAS HEC-RAS 5.0.7 March 2019 U.S. Army Corps of Engineers Hydrologic Engineering Center 609 Second Street Davis, California

х	х	XXXXXX	XX	XX		XX	XX	X	X	XXXX
X	×	x	X	X		X	х	X	Х	x
х	х	X	х			X	Х	х	X	X
XXXX	XXXX	XXXX	X		XXX	XX	XX	XXX	XXX	XXXX
х	х	Х	X			X	X	х	X	x
Х	Х	Х	х	Х		X	Х	Х	Х	Х
X	X	XXXXXX	XX	XX		X	X	Х	Х	XXXXX

PROJECT DATA

Project Title: Butteville Dock Project File : ButtevilleDock.prj Run Date and Time: 5/3/2020 1:30:28 PM

Project in English units

PLAN DATA

Plan Title: Plan 08

Plan File : p:\2020 Small Jobs\Butterville Landing\HEC-RAS\ButtevilleDock.p08

Geometry Title: floodplain site adjusted bottom L

Geometry File: p:\2020 Small Jobs\Butterville Landing\HEC-RAS\ButtevilleDock.g07

: Precondition adj bottom to FEMA Flow Title

: p:\2020 Small Jobs\Butterville Landing\HEC-RAS\ButtevilleDock.f02 Flow File

Plan Summary Information:

Number of: Cross Sections = 4 Multiple Openings = 0 Culverts = 0 Inline Structures = 0 Bridges 0 Lateral Structures = 0

Computational Information

Water surface calculation tolerance = 0.01 Critical depth calculation tolerance = 0.01 Maximum number of iterations **≈** 20 Maximum difference tolerance ≈ 0.3 Flow tolerance factor = 0.001

Computation Options

Critical depth computed only where necessary

Conveyance Calculation Method: At breaks in n values only

Friction Slope Method: Computational Flow Regime: Average Conveyance

Subcritical Flow

FLOW DATA

Flow Title: Precondition adj bottom to FEMA

Flow File: p:\2020 Small Jobs\Butterville Landing\HEC-RAS\ButtevilleDock.f02

Flow Data (cfs)

10 yr 50 yr 100 yr Reach RS River 182000 260000 302000 Butteville 43.30 Willamette R

#### Boundary Conditions

River Downstream		Reach	Profile	Upstream
Willamette = 82.8	R	Butteville	10 yr	Known WS
Willamette = 90.7	R	Butteville	50 yr	Known WS
Willamette = 94.1	R	Butteville	100 yr	Known WS

#### GEOMETRY DATA

Geometry Title: floodplain site adjusted bottom L Geometry File: p:\2020 Small Jobs\Butterville Landing\HEC-RAS\ButtevilleDock.g07

CROSS SECTION

RIVER: Willamette R

RS: 43.30 REACH: Butteville

INPUT									
Descripti	on: E Se	ction							
Station E	levation	Data	กนฑ≕	77					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	105.46	9.09	104.27	11.03	104	11.35	104	30.85	102.58
36.08	102.2	38.88	102	43.2	100.36	43.77	100.09	44.12	100
49.1	98.05	49.23	98	54.27	96.03	54,34	96	59.37	94.03
59,46	94	64.46	92.04	64.57	92	69.54	90.06	69.68	90
74.58	88.08	74.8	88	79.51	86,16	79.91	86	80.99	85.52
83.57	84	85.37	83.02	86.34	82.57	87,58	82	88.1	81.76
88.42	81.62	90.19	80.91	92	80.2	92.35	80	94.2	78.93
95,61	78	96.6	77.35	98.65	76	100.88	74.54	101.7	74
104.61	72.09	104.74	72	105.52	71.49	107.64	70.29	108.15	70
110.31	68.78	111.68	68	112.68	67.43	113,99	66.69	114,67	66.37
115,43	66	116.26	65.6	116.59	65.45	118.69	64	119.32	63.57
121.6	62	124,24	60.22	124.56	60	192,4	52	294.3	42
420	7.5	500	7.5	600	41.87	702	52	742.8	54
787.47	60	788.86	60.5	793.05	62	794.08	62,37	807.6	70
828.4	80	853.4	90	881.9	96	900	96.6	917.8	96
944.5	94	1018,2	92						
Manning's	n Value	s	num=	3					

Manning's	n Value	s	num=	3	
Sta	n Val	Sta	n Val	Sta	n Val
0	.07	124.56	.033	787.47	.05

 Bank Sta: Left
 Right
 Lengths: Left Channel
 Right
 Coeff Contr.
 Expan.

 124.56
 787.47
 1583.2
 1636.8
 1756.1
 .1
 .3

CROSS SECTION OUTPUT Profile #10 yr

E.G. Elev (ft)	83.54	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.53	Wt. n-Val.	0.070	0.033	0.050
W.S. Elev (ft)	83.00	Reach Len. (ft)	1583.20	1636,80	1756.10
Crit W.S. (ft)		Flow Area (sq ft)	428.97	30759.60	549.33
E.G. Slope (ft/ft)	0.000105	Area (sq ft)	428.97	30759.60	549.33
Q Total (cfs)	182000.00	Flow (cfs)	415.74	180797.10	787.17
Top Width (ft)	750.50	Top Width (ft)	39.15	662.91	48.44
Vel Total (ft/s)	5.73	Avg. Vel. (ft/s)	0.97	5.88	1.43
Max Chl Dpth (ft)	75.50	Hydr. Depth (ft)	10,96	46.40	11.34
Conv. Total (cfs)	17784260.0	Conv. (cfs)	40623.9	17666720.0	76918.8
Length Wtd. (ft)	1637.17	Wetted Per. (ft)	45.52	675.21	53.71
Min Ch El (ft)	7.50	Shear (lb/sq ft)	0.06	0.30	0.07
Alpha	1.04	Stream Power (1b/ft s)	0.06	1.75	0.10
Frctn Loss (ft)	0.14	Cum Volume (acre-ft)	48.75	2562.11	56.00
C & E Loss (ft)	0.03	Cum SA (acres)	4.08	49.43	5.71

#### CROSS SECTION OUTPUT Profile #50 yr

E.G. Elev (ft)	91.74	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.78	Wt. n-Val.	0.070	0.033	0.050
W.S. Elev (ft)	90.96	Reach Len. (ft)	1583.20	1636.80	1756.10
Crit W.S. (ft)		Flow Area (sq ft)	807.21	36033.63	1014.84
E.G. Slope (ft/ft)	0.000125	Area (sq ft)	807.21	36033.63	1014.84
O Total (cfs)	260000.00	Flow (cfs)	1023.03	257099.20	1877.83
Top Width (ft)	790.72	Top Width (ft)	57.32	662,91	70.48
Vel Total (ft/s)	6.87	Avg. Vel. (ft/s)	1.27	7.13	1.85
Max Chl Dpth (ft)	83.46	Hydr. Depth (ft)	14.08	54.36	14.40
Conv. Total (cfs)	23258100.0	Conv. (cfs)	91514.6	22998600.0	167980.0
Length Wtd. (ft)	1637.59	Wetted Per. (ft)	65.40	675.21	77.21
Min Ch El (ft)	7.50	Shear (lb/sq ft)	0.10	0.42	0.10
Alpha	1.07	Stream Power (lb/ft s)	0.12	2.97	0.19
Fretn Loss (ft)	0.18	Cum Volume (acre-ft)	86.79	2954.26	115.40
C & E Loss (ft)	0.03	Cum SA (acres)	5.55	49.43	8.76

#### CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	95.32	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.93	Wt. n-Val.	0.070	0.033	0.050
W.S. Elev (ft)	94.39	Reach Len. (ft)	1583.20	1636.80	1756.10
Crit W.S. (ft)		Flow Area (sq ft)	1019.04	38308.94	1388.29
E.G. Slope (ft/ft)	0.000137	Area (sq ft)	1019.04	38308.94	1388.29
Q Total (cfs)	302000.00	Flow (cfs)	1443.04	297958.90	2598.01
Top Width (ft)	894.73	Top Width (ft)	66.11	662.91	165.71
Vel Total (ft/s)	7.42	Avg. Vel. (ft/s)	1.42	7.78	1.87
Max Chl Doth (ft)	86.89	Hydr, Depth (ft)	15,41	57.79	8.38
Conv. Total (cfs)	25815010.0	Conv. (cfs)	123351.6	25469580.0	222078.5
Length Wtd. (ft)	1637.83	Wetted Per. (ft)	74.84	675.21	175.22
Min Ch El (ft)	7.50	Shear (lb/sq ft)	0.12	0.48	0.07
Alpha	1.09	Stream Power (lb/ft s)	0.16	3.77	0.13
Fretn Loss (ft)	0.19	Cum Volume (acre-ft)	106.87	3123.31	149.40
C & E Loss (ft)	0.04	Cum SA (acres)	6.20	49.43	11.51

Warning: Divided flow computed for this cross-section.
Warning: The cross-section end points had to be extended vertically for the computed water surface.

CROSS SECTION

RIVER: Willamette R

REACH: Butteville RS: 42.99

INPUT									
Descripti	on: D Se	ction							
Station E	Elevation	Data	num=	100					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	110.01	6.48	110.01	6.55	110	6.58	110	6.6	110
6.78	109.98	19.56	108.6	23.01	108.26	25.45	108	25.95	107.93
32.85	106	36.92	104.83	39.83	104	43.5	102.95	49.84	101.14
53.81	100	56.1	99.34	60.79	98	62.25	97.58	67.78	96
68.27	95.86	70.96	95.09	73.59	94	74.03	93.82	78.42	92
79.49	91.56	83.25	90	84.79	89.36	88.08	88	89.98	B7.21
92.91	86	95.11	85.09	97.74	84	100,18	82.99	102.57	82
105.2	80.91	107.41	80	110.2	78.84	112.24	78	115.18	76.78
117.07	76	120.13	74.73	121.9	74	125.07	72.69	126.73	72
128.7	71.18	131.56	70	134.01	68.99	136.39	68	139.61	66.67
141,22	66	145,92	64.05	146.05	64	146.33	63.88	146.55	63.85
147.74	63.74	148.83	63.53	156.85	62.4	159.67	62	169	60.68
173.81	60	211	28.52	294.3	26	414.3	25.2	525.1	25.2
629.2	26	729	28.06	793.47	60	794.55	60.48	799.77	62
799.91	62,04	807.67	64	820,15	67.16	B23.47	68	830.91	70
841.29	74	851.68	78	856,88	80	857.06	80.07	857.98	80.22
866.14	81.52	874.77	82	888.63	82.76	911.1	84	930.42	85.06

935.17 86 936.33 965.32 91.92 965.68			88.89 955.54 94 978.32		
965.32 91.92 965.68 984.79 96 989.73			98.9 1002.6		
Manning's n Values		3			
Sta n Val Sta 0 .07 173.81		Sta n Val .47 .05			
0 .07 173.81	.033 193	.47 .05			
Bank Sta: Left Right	Lengths: Le		Coeff Contr.		
173.81 793.47	316	.3 316.4 316.8	.1	.3	
CROSS SECTION OUTPUT Pro	ofile #10 yr				
E.G. Elev (ft)	83.37	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.45	Wt. n-Val.	0.070	0.033	0.050
W.S. Elev (ft) Crit W.S. (ft)	82.92	Reach Len. (ft) Flow Area (sq ft)	316.30 1014.12	316.40 33401.13	316.80 909.23
E.G. Slope (ft/ft)	0.000073	Area (sq ft)	1014.12	33401.13	909.23
Q Total (cfs)	182000.00	Flow (cfs)	1022.74	179979.50	997.74
Top Width (ft)	791.21	Top Width (ft)	73.47	619.66	98.09
Vel Total (ft/s)	5.15	Avg. Vel. (ft/s)	1.01	5.39	1.10
Max Chl Dpth (ft)	57.72	Hydr. Depth (ft)	13.80		
Conv. Total (cfs)	21267500.0	Conv. (cfs)	119511.7		0 116590.5
Length Wtd. (ft)	316.40	Wetted Per. (ft)	77.53		101.45
Min Ch El (ft) Alpha	25.20 1.08	Shear (lb/sq ft) Stream Power (lb/ft s	0.06	0.24 1.29	0.04 0.04
Fretn Loss (ft)	1.08 0.02	Cum Volume (acre-ft)		1356.67	26.60
C & E Loss (ft)	0.00	Cum SA (acres)	2.04	25.34	2.76
CROSS SECTION OUTPUT Pr	ofile #50 yr				
E.G. Elev (ft)	91.53	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.67	Wt. n-Val.	0.070	0.033	0.050
W.S. Elev (ft)	90.86	Reach Len. (ft)	316.30	316.40	316.80
Crit W.S. (ft)		Flow Area (sq ft)	1673.45	38320.38	2040.36
E.G. Slope (ft/ft)	0.000093	Area (sq ft)	1673.45	38320.38	2040.36
Q Total (cfs)	260000.00	Flow (cfs)	2264.47 92.63	254679.30 619.66	3056.19 166.45
Top Width (ft) Vel Total (ft/s)	878.75 6.19	Top Width (ft) Avg. Vel. (ft/s)	1.35	6.65	1.50
Max Chl Dpth (ft)	65.66	Hydr. Depth (ft)	18.07	61.84	12.26
Conv. Total (cfs)	26995760.0	Conv. (cfs)	235120.0		0 317323.7
Length Wtd. (ft)	316.40	Wetted Per. (ft)	98.27	638.74	170.43
Min Ch El (ft)	25.20	Shear (lb/sq ft)	0.10	0.35	0.07
Alpha	1.13	Stream Power (lb/ft s		2.31	0.10
Fretn Loss (ft)	0.03	Cum Volume (acre-ft)			53.82
C & E Loss (ft)	0.00	Cum SA (acres)	2.82	25.34	3.98
CROSS SECTION OUTPUT Pro	ofile #100 yr				
E.G. Elev (ft)	95.09	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.80	Wt. n-Val.	0.070		0.050
W.S. Elev (ft)	94.28	Reach Len. (ft)	316.30	316.40	316.80
Crit W.S. (ft)	0.000100	Flow Area (sq ft)	2004.83	40442.36	2639.12
E.G. Slope (ft/ft)	0.000103	Area (sq ft) Flow (cfs)	2004.83 3049.82	40442.36 294295.30	2639.12 4654.92
Q Total (cfs) Top Width (ft)	302000.00 903.52	Top Width (ft)	100.91	619.66	182.95
Vel Total (ft/s)	6.70	Avg. Vel. (ft/s)	1.52	7.28	1.76
Max Chl Dpth (ft)	69.08	Hydr. Depth (ft)	19.87	65.27	14.43
Conv. Total (cfs)	29685940.0	Conv. (cfs)	299790.5	28928580.	
Length Wtd. (ft)	316.40	Wetted Per. (ft)	107.23	638.74	187.28
Min Ch El (ft)	25.20	Shear (lb/sq ft)	0.12	0.41	0.09
Alpha	1,15	Stream Power (1b/ft s	•	2.98	0.16
Fretn Loss (ft)	0.03 0.00	Cum Volume (acre-ft) Cum SA (acres)	51.91 3.17	1643.74 25.34	68.22 4.48
C & E Loss (ft)	0.00	omm ou factes)	3,11	HU 1 U 3	4.10

RIVER: Willamette R

REACH: Butteville	RS: 42.93						
INPUT							
Description: Upstream							
Station Elevation Date		73					
	Sta Elev	Sta Elev		Elev	Sta		
		2.37 102 3.06 99.14	23.41 62.22	102 98	29.9 63.11	101.36 98	
		1.06 94	75.13	92	79.2	90	
63.66 97.63 66 83.27 88 87		7.82 85.77	90.85	84	94.29		
97.6 80 101					111,44	72	
114.9 70 114			124.06		127.33		
127.81 62 128		1.25 60	170	26.52	294.3		
414.3 25.1 52		680 26.15		43.38	729.2		
735.26 47.34 745			760.64	57.56	763.5		
763.63 60 776			785.38		786.02		
796.82 71.4 806	.08 74.49 81	0.33 75.46	819.71	76.78	828,27	78.93	
834.82 79.7 840,	199 81.11 84	7.62 82.71	859.14	84.92	864.18	85.61	
880.6 89.7 885	.18 90.96 89	8.11 94	911,16	96	923,22		
937.25 100 945			970.48	102.44	971.36	102.39	
978.01 102 998	.15 102 99	9.16 102					
		_					
Manning's n Values	num=	3					
	Sta n Val	Sta n Val					
0 .07 131	.25 .033 76	3.63 .05					
Bank Sta: Left Right	. Jonatha I	eft Channel	Pight	Coeff	Contr	Expan.	
Bank Sta: Left Right 131.25 763.6			1448	COGIL	,1	.3	
131.23 703.0	*	101 1120	1110		1 **		
CROSS SECTION OUTPUT	Profile #10 vr						
J							
E.G. Elev (ft)	83.34	Element		L	eft OB	Channel	Right OB
Vel Head (ft)	0.44	Wt. n-Val.		Í	0.070	0.033	0.050
W.S. Elev (ft)	82.91	Reach Len.	(ft)	14	04.00	1426.00	1448.00
Crit W.S. (ft)		Flow Area	(sq ft)		39.17	33992.04	767.75
E.G. Slope (ft/ft)		Area (sq fi			39.17	33992.04	767.75
Q Total (cfs)	182000.00	Flow (cfs)			361.89	180838.00	800.15
Top Width (ft)	755.90	Top Width			38.52	632.38	85.01
Vel Total (ft/s)	5.17	Avg, Vel.	(it/s)		0.82	5.32	1.04
Max Chl Dpth (ft)	57.81	Hydr. Deptl			11.40	53.75	9.03
Conv. Total (cfs)	21462150.0				42675.1 44.84	21325120. 653.62	0 94356.5 91.29
Length Wtd. (ft)	1426.03 25.10	Wetted Per Shear (lb/s			0.04	0.23	0.04
Min Ch El (ft) Alpha	1.05	Stream Power			0.04	1.24	0.04
Fretn Loss (ft)	0.10	Cum Volume			17.25		20.50
C & E Loss (ft)	0.00	Cum SA (acı			1.63	20.79	2.09
0 4 1 2000 (20)	*****	J. 21. (40.	,		-100		
CROSS SECTION OUTPUT	Profile #50 yr						
E.G. Elev (ft)	91.50	Element		Ŀ	eft OB	Channel	Right OB
Vel Head (ft)	0.66	Wt. n-Val.			0.070	0.033	0.050
W.S. Elev (ft)	90.84	Reach Len.			04.00	1426.00	1448.00
Crit W.S. (ft)		Flow Area				39007.99	1597.43
E.G. Slope (ft/ft)	0.000092	Area (sq fi			02.80	39007.99	1597.43
Q Total (cfs)	260000.00	Flow (cfs)			898.88	256660.70	2440.39
Top Width (ft)	807.24	Top Width	• •	•	53,75	632.38	121,10
Vel Total (ft/s)	6.28	Avg. Vel.			1.12 14.93	6.58 61.68	1,53 13,19
Max Chl Dpth (ft)	65.74 27172700.0	Hydr. Depth Conv. (c:			93942.1	26823710.	
Conv. Total (cfs) Length Wtd. (ft)	1426.06	Wetted Per			62.03	653,62	128.28
Min Ch El (ft)	25.10	Shear (lb/s			0.07	0.34	0.07
Alpha	1.08	Stream Powe		s)	0.08	2,24	0.11
Fretn Loss (ft)	0.13	Cum Volume			32,72	1276,47	40.59
C & E Loss (ft)	0.00	Cum SA (acı		•	2.29	20.79	2.94
			•				

Left OB

Channel Right OB

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft) 95.05 Element

Vel Head (ft) W.S. Elev (ft) Crit W.S. (ft) E.G. Slope (ft/ft) Q Total (cfs) Top Width (ft) Vel Total (ft/s) Max Chl Dpth (ft) Conv. Total (cfs) Length Wtd. (ft) Min Ch El (ft) Alpha Fretn Loss (ft) C & E Loss (ft)	0.80 94.26 0.000103 302000.00 829.24 6.83 69.16 29826480.0 1426.08 25.10 1.10 0.15 0.00	Wt. n-Val. Reach Len. (ft) Flow Area (sq ft) Area (sq ft) Flow (cfs) Top Width (ft) Avg. Vel. (ft/s) Hydr. Depth (ft) Conv. (cfs) Wetted Per. (ft) Shear (lb/sq ft) Stream Power (lb/ft Cum Volume (acre-ft) Cum SA (acres)	60.71 1.27 16.45 124925.5 69.78 0.09 s) 0.12	0.033 0.050 1426.00 1448.00 41170.18 2036.18 41170.18 2036.18 297147.70 3587.41 632.38 136.15 7.22 1.76 65.10 14.96 29347250.0 354303.6 653.62 143.72 0.40 0.09 2.91 0.16 1347.35 51.22 20.79 3.32
CROSS SECTION				
RIVER: Willamette R REACH: Butteville	RS: 42.66			
INPUT				
Description: C section				
Station Elevation Data		6	-	
Sta Elev Sta		Sta Elev Sta	Elev Sta	
0 98.73 6.85		.33 94 21.82	92 34.8 82 60.75	88 80
38.86 86.75 41.29 60.82 80 68.07		.78 84 54.26 .78 78 69.39	77.84 69.51	
69.82 77.7 71.07		.18 76 75.8	75.79 81.09	
86.94 72 92.2		.89 66 102.82	65.62 106.55	64
111.01 62.2 111.05		.25 61.88 113.92	60.22 114.31	60
187 29.5 294.3	25.5 41	4,3 25,1 525,1	25.1 629.2	
705 29.06 751.96	60 759 80 794	4.3 25.1 525.1 .12 64 766.29 .94 84 802.1 .48 96 832.03	68 773.45	
780.61 76 787.78	80 794	.94 84 802.1	88 810.09	
813.49 93.66 814.93			98 849.12	
854.84 103.34 859.57	103.4 875	.15 103.03 877.1	103.05 881.32	102.91
894.09 102.64				
Manning's n Values	num=	3		
Sta n Val Sta		Sta n Val		
0 .07 114.31	.033 751	.96 .05		
Bank Sta: Left Right		· · · · · · · · · · · · · · · · · · ·		
114.31 751.96	.1	.3		
CROSS SECTION OUTPUT Pro	file #10 ur			
CROSS SECTION OUTFOIL FIX	STITE MIG AT			
E.G. Elev (ft)	83.24	Element	Left OB	Channel Right OB
Vel Head (ft)	0.44	Wt. n-Val.	0.070	0.033 0.050
W.S. Elev (ft)	82.80	Reach Len. (ft)		
Crit W.S. (ft)	41,60	Flow Area (sq ft)	631.26	33939.06 465.47
E.G. Slope (ft/ft)	0.000072	Area (sq ft)	631.26	
Q Total (cfs)	182000.00	Flow (cfs)	508,62	180947.10 544.29
Top Width (ft) Vel Total (ft/s)	741.12 5.19	Top Width (ft) Avg. Vel. (ft/s)	62.64 0.81	637.65 40.83 5,33 1.17
Max Chl Dpth (ft)	57.70	Hydr. Depth (ft)	10.08	53.23 11.40
Conv. Total (cfs)	21402630.0	Conv. (cfs)	59812,1	
Length Wtd. (ft)		Wetted Per. (ft)	66.94	653.21 46.77
Min Ch El (ft)	25,10	Shear (lb/sq ft)	0.04	0.23 0.04
Alpha	1.05	Stream Power (lb/ft		1.25 0.05
Frotn Loss (ft)		Cum Volume (acre-ft	<b>)</b>	
C & E Loss (ft)		Cum SA (acres)		
CROSS SECTION OUTPUT Pro	ofile #50 yr			
	• • • • •	<b>51</b>	* ** **	ghannal might on
E.G. Elev (ft)	91.37	Element	Left OB	Channel Right OB 0.033 0.050
Vel Head (ft) W.S. Elev (ft)	0.67 90.70	Wt. n-Val. Reach Len. (ft)	0.070	0.033 0.050
w.s. Elev (It) Crit W.S. (ft)	45.71	Flow Area (sq ft)	1227.34	38976.49 844.66
OIIG 8:0: (IU)	70:14	(Dd)		

E.G. Slope (ft/ft) Q Total (cfs) Top Width (ft) Vel Total (ft/s) Max Chl Dpth (ft) Conv. Total (cfs) Length Wtd. (ft) Min Ch El (ft) Alpha	0,000092 260000.00 781.45 6.33 65.60 27084710.0 25.10 1.07	Area (sq ft) Flow (cfs) Top Width (ft) Avg. Vel. (ft/s) Hydr. Depth (ft) Conv. (cfs) Wetted Per. (ft) Shear (lb/sq ft) Stream Power (lb/ft s)	1227.34 1389.15 88.27 1.13 13.90 144710.2 93.76 0.08 0.09	38976.49 257257.50 637.65 6.60 61.13 26799020.0 653.21 0.34 2.27	844.66 1353.35 55.53 1.60 15.21 140981.4 63.46 0.08 0.12
• •					

#### CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	94.91	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.81	Wt. n-Val.	0.070	0.033	0.050
W.S. Elev (ft)	94.10	Reach Len. (ft)			
Crit W.S. (ft)	47.66	Flow Area (sq ft)	1546.22	41144.50	1045.34
E.G. Slope (ft/ft)	0.000103	Area (sq ft)	1546.22	41144.50	1045.34
Q Total (cfs)	302000.00	Flow (cfs)	2000.54	298121.30	1878.14
Top Width (ft)	800.35	Top Width (ft)	99.30	637,65	63.40
Vel Total (ft/s)	6.91	Avg. Vel. (ft/s)	1.29	7.25	1.80
Max Chl Dpth (ft)	69.00	Hydr. Depth (ft)	15.57	64.53	16.49
Conv. Total (cfs)	29710820.0	Conv. (cfs)	196813.8	29329240.0	184771.5
Length Wtd. (ft)		Wetted Per. (ft)	105.30	653.21	72.07
Min Ch El (ft)	25.10	Shear (lb/sq ft)	0.09	0.41	0.09
Alpha	1.09	Stream Power (lb/ft s)	0.12	2.94	0.17
Fretn Loss (ft)		Cum Volume (acre-ft)			
C & E Loss (ft)		Cum SA (acres)			

#### SUMMARY OF MANNING'S N VALUES

#### River: Willamette R

Reach	River Sta.	n1	n2	n3
Butteville	43.30	.07	.033	. 05
Butteville	42.99	.07	.033	.05
Butteville	42.93	.07	.033	.05
Butteville	42,66	.07	.033	.05

#### SUMMARY OF REACH LENGTHS

River: Willamette R

Reach	River Sta.	Left	Channel	Right
Butteville	43,30	1583.2	1636.8	1756.1
Butteville	42.99	316.3	316.4	316.8
Butteville	42.93	1404	1426	1448
Butteville	42.66			

# SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS River: Willamette $\ensuremath{\mathtt{R}}$

Reach	River Sta.	Contr.	Expan
Butteville Butteville Butteville	43.30 42.99 42.93	.1 .1	.3 .3

Profile Output Table - Standard Table 1

Butteville

Reach	<b>1</b>	River	Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G.
Elev	E.G. Slop	e Ve	el Chnl	Flow Area	Top Widtl	r Froude #	Chl	(ft)	
	10.10.		1.04.1-1	(n 61)	(CIS)	(ft)	(It)	(IT)	
Butte	ville .	43.30		10 yr	182000.00	7.50	83.00		
83.54	0.0001	05	5,88	31737.9	0 750.5	50	0.15		
Butte	eville	43.30		50  yr	260000.00	7.50	90.96		
91.74	0.0001	25	7.13	37855.6	8 790.7	12	0.17		
Butte	eville	43.30		100 yr	302000.00	7.50	94.39		
95.32	0.0001	37	7.78	10 yr 31737.96 50 yr 37855.66 100 yr 40716.2	7 894.	73	0.18		
Butte	ville	42.99		10 yr 35324.4 50 yr 42034.1 100 yr 45086.3	182000.00	25.20	82.92		
83.37	0.0000	73	5.39	35324.4	8 791.2	21	0.13		
Butte	ville	42.99		50 yr :	260000.00	25.20	90.86		
91.53	0.0000	93	6.65	42034.1	8 878.7	75	0.15		
Butte	eville	42.99		100 yr	302000.00	25.20	94.28		
Butte	eville	42.93		10 yr 35198.9 50 yr 41408.2 100 yr 44204.8	182000.00	25.10	82.91		
83.34	0.0000	72	5.32	35198.9	6 755.9	90	0.13		
Butte	ville	42.93		50 yr	260000.00	25.10	90.84		
91.50	0.0000	92	6.58	41408.2	3 807.2	24	0.15		
Butte	eville	42.93		100 yr	302000.00	25.10	94.26		
Butte	eville	42.66		10 yr	182000.00	25.10	82.80	41.60 45.71 47.66	
83.24	0.0000	72	5.33	35035.7	9 741.3	L2	0.13		
Butte	ville	42.66		50 yr	260000.00	25,10	90.70	45,71	
91.37	0.0000	92	6.60	41048.4	9 781.	15	0.15		
Butte	ville	42.66		100 yr	302000.00	25.10	94.10	47.66	
94.91	0.0001	03	7.25	43736.0	6 800.3	35	0.16		

#### WITH DOCK

HEC-RAS HEC-RAS 6.1.0 September 2021 U.S. Army Corps of Engineers Hydrologic Engineering Center 609 Second Street Davis, California

Х	Х	XXXXXX	ХХ	XX		XX	XX	>	X	XXXX
Х	Х	x	Х	Х		Х	Х	Х	Х	X
X	X	X	Х			Х	Х	X	X	X
XXX	XXXX	XXXX	X		XXX	XX	XX	XXX	XXX	XXXX
Х	Х	X	Х			Х	X	X	Х	X
Х	X	X	Х	Х		Х	Х	X	х	X
X	X	XXXXXX	XX	XX		Х	Х	X	X	XXXXX

PROJECT DATA

Project Title: Butteville D Lan UpSt Project File: ButtevilleDockLan.prj Run Date and Time: 12/13/2021 9:32:07 AM

Project in English units

Project Description: Upstream Face of Dock

#### PLAN DATA

Plan Title: Plan 14

Plan File: p:\2020 Small Jobs\Butterville Landing\HEC-RAS\ButtevilleDockLan.p14

Geometry Title: floodplain+dock site adjusted bottom L

Geometry File : p:\2020 Small Jobs\Butterville Landing\HEC-RAS\ButtevilleDockLan.g08

Flow Title : Precondition adj bottom to FEMA

Flow File : p:\2020 Small Jobs\Butterville Landing\HEC-RAS\ButtevilleDockLan.f02

Plan Description:

case with 12" piler upstream

Plan Summary Information:

Number of: Cross Sections = 4 Multiple Openings = 0
Culverts = 0 Inline Structures = 0
Bridges = 0 Lateral Structures = 0

Computational Information

Water surface calculation tolerance = 0.01
Critical depth calculation tolerance = 0.01
Maximum number of iterations = 20
Maximum difference tolerance = 0.3
Flow tolerance factor = 0.001

Computation Options

Critical depth computed only where necessary

Conveyance Calculation Method: At breaks in n values only

Friction Slope Method:

Average Conveyance

Computational Flow Regime:

Subcritical Flow

Flow Title: Precondition adj bottom to FEMA

Flow File : p:\2020 Small Jobs\Butterville Landing\HEC-RAS\ButtevilleDockLan.f02

Flow Data (cfs)

River	Reach	RS	10 yr	50 yr	100 yr
Willamette R	Butteville	43.30	182000	260000	302000

#### **Boundary Conditions**

River	Reach	Profile	Upstream	Downstream
Willamette R	Butteville	10 yr		Known WS = 82.8
Willamette R	Butteville	50 yr		Known WS = 90.7
Willamette R	Butteville	100 yr		Known WS = 94.1

Sta

30.85

Elev

102.58

#### GEOMETRY DATA

Geometry Title: floodplain+dock site adjusted bottom L

Geometry File : p:\2020 Small Jobs\Butterville Landing\HEC-RAS\ButtevilleDockLan.g0B

CROSS SECTION

RIVER: Willamette R

REACH: Butteville RS: 43.30

INPUT

Description: E Section 77 Station Elevation Data num= Sta Sta Elev Sta Elev Elev Sta Elev 11.35 104 11.03 104 105.46 9.09 104.27 36.08 102.2 38.88 102 43.2 100.36 43.77 96.03 54.34 49.1 98,05 49,23 98 54.27

100.09 44.12 100 96 59.37 94.03 92 69.54 90.06 69.68 59.46 92.04 64.57 94 64.46 79.91 80.99 85.52 86 74.58 88.08 74.8 88 79.51 86,16 82 88.1 81,76 83.57 84 85.37 83.02 86.34 82.57 87.58 88.42 81.62 90.19 80.91 92 80.2 92.35 80 94.2 78.93 98.65 76 100.88 74.54 101.7 74 77.35 95.61 96.6 78 70 70.29 108.15 72.09 105.52 71,49 107.64 104.61 104.74 72 114.67 66.37 110.31 68.78 111.68 68 112.68 67.43 113.99 66.69 115.43 66 116.26 65.6 116.59 65,45 118.69 64 119.32 63.57 192.4 52 294.3 42 60.22 124.56 60 121.6 62 124.24 702 52 742.8 54 41.87 7.5 699 425.5 7.5 500 62 794.08 807.6 787,47 60 788.86 60.5 793.05 62.37 70 80 853.4 90 881.9 96 900 96.6 917.8 96 828.4 944.5 94 1018.2 92

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
0 .07 124.56 .033 787.47 .05

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan. 124.56 787.47 1583.2 1636.8 1756.1 .1 .3

#### CROSS SECTION OUTPUT Profile #10 yr

E.G. Elev (ft)	83.55	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.54	Wt. n-Val.	0.070	0.033	0.050
W.S. Elev (ft)	83.01	Reach Len. (ft)	1583.20	1636,80	1756.10
Crit W.S. (ft)		Flow Area (sq ft)	429.29	30670.11	549.72
E.G. Slope (ft/ft)	0.000106	Area (sq ft)	429.29	30670.11	549.72
O Total (cfs)	182000.00	Flow (cfs)	418.06	180790.40	791.55
Top Width (ft)	750.54	Top Width (ft)	39.17	662.91	48.46

Vel Total (ft/s)	5.75	Avg, Vel. (ft/s)	0.97	5.89	1.44
Max Chl Doth (ft)	75.51	Hydr. Depth (ft)	10,96	46.27	11.34
Conv. Total (cfs)	17702060.0	Conv. (cfs)	40662.6	17584410.0	76989.8
Length Wtd. (ft)	1637.17	Wetted Per. (ft)	45.54	675.02	53.73
Min Ch El (ft)	7.50	Shear (1b/sq ft)	0.06	0.30	0.07
Alpha	1.04	Stream Power (1b/ft s)	0.06	1.77	0.10
Fretn Loss (ft)	0.14	Cum Volume (acre-ft)	48.78	2559.88	56.04
C & E Loss (ft)	0.03	Cum SA (acres)	4.08	49.41	5.72
		•			
CROSS SECTION OUTPUT	Profile #50 yr				
E.G. Elev (ft)	91.76	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.79	Wt. n-Val.	0.070	0,033	0.050
W.S. Elev (ft)	90,97	Reach Len. (ft)	1583.20	1636.80	1756.10
Crit W.S. (ft)		Flow Area (sq ft)	807.96	35947.40	1015.76
E.G. Slope (ft/ft)	0.000126	Area (sq ft)	807.96	35947.40	1015.76
O Total (cfs)	260000.00	Flow (cfs)	1028.09	257085.20	1886,71
Top Width (ft)	790.81	Top Width (ft)	57.36	662.91	70.55
Vel Total (ft/s)	6.88	Avg. Vel. (ft/s)	1,27	7.15	1.86
Max Chl Dpth (ft)	83.47	Hydr, Depth (ft)	14.09	54.23	14.40
Conv. Total (cfs)	23170980.0	Conv. (cfs)	91622.4	22911210.6	168141.8
Length Wtd. (ft)	1637.60	Wetted Per. (ft)	65.44	675.02	77.27
Min Ch El (ft)	7,50	Shear (1b/sq ft)	0.10	0.42	0.10
Alpha	1.07	Stream Power (lb/ft s)	0.12	2.99	0.19
Fretn Loss (ft)	0.18	Cum Volume (acre-ft)	86.85	2952.07	115.51
C & E Loss (ft)	0.03	Cum SA (acres)	5.55	49.41	8.76
	n				
CROSS SECTION OUTPUT	Profile #100 At	•			
E.G. Elev (ft)	95.34	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.93	Wt. n-Val.	0.070	0.033	0.050
W.S. Elev (ft)	94.41	Reach Len. (ft)	1583.20	1636.80	1756.10
Crit W.S. (ft)		Flow Area (sq ft)	1020.11	38224.77	1390.97
<pre>E.G. Slope (ft/ft)</pre>	0.000138	Area (sq ft)	1020.11	38224.77	1390.97
Q Total (cfs)	302000 <b>.0</b> 0	Flow (cfs)	1449.94	297939.20	2610.93
Top Width (ft)	895.06	Top Width (ft)	66.15	662.91	166.00
Vel Total (ft/s)	7.43	Avg. Vel. (ft/s)	1.42	7.79	1.88
Max Chl Dpth (ft)	86.91	Hydr. Depth (ft)	15.42	57.66	8.38
Conv. Total (cfs)	25727040.0	Conv. (cfs)	123518.3		
Length Wtd. (ft)	1637.84	Wetted Per. (ft)	74.88	675.02	175.53
Min Ch El (ft)	7.50	Shear (1b/sq ft)	0.12	0.49	0.07
Alpha	1.09	Stream Power (lb/ft s)	0.17	3.80	0.13

Warning: Divided flow computed for this cross-section.

0.19

0.04

Warning: The cross-section end points had to be extended vertically for the computed water surface.

Cum Volume (acre-ft)

Cum SA (acres)

149.58

11.52

3121.19

49,41

106.95 6.20

#### **CROSS SECTION**

RIVER: Willamette R

Frctn Loss (ft)
C & E Loss (ft)

REACH: Butteville RS: 42.99

INPUT

Description: D Section 100 Station Elevation Data กยต= Elev Elev Sta Elev Sta Elev Sta Elev Sta Sta 6.55 110 6.58 110 6.6 110 110.01 6.48 110.01 0 23.01 108.26 25.45 108 25.95 107.93 108.6 6.78 109.98 19.56 102.95 49.84 101.14 43.5 104.83 39.83 104 32.85 106 36,92 67.78 96 98 62.25 97.58 53.81 100 56.1 99.34 60.79 92 95.86 70.96 95.09 73.59 94 74.03 93.82 78.42 68.27 88.08 88 89.98 87.21 90 84,79 89.36 79,49 83.25 91.56 82.99 102.57 82 100.18 84 85.09 97.74 92.91 86 95.11 78 115.18 76.78 78.84 112.24 105.2 80.91 107.41 80 110.2

117.07						400 07	70 60	446 73			
		120.13	74.73	121		125.07		126.73	72		
128.7		131.56		134.				139.61			
141.22	66	145.92	64.05	146.	<b>05 64</b>	146.33	63.88	146.55	63.85		
147.74	63.74	148.83	63.53	156.	85 62.4	159.67	62	169	60.68		
173.81	60	211	28.52	294	.3 26	414.3	25.2	525.1	25.2		
629.2	26	72 <del>9</del>	28.06	793.	47 60	794.55	60.48	799.77	62		
799.91		807.67		820.				830.91	70		
841.29		851.68		856.		857.06		857.98			
866.14		874.77		888.		911.1		930.42			
								955.54			
935.17		936.33	86.22			949.91					
965.32		965.68		965.		975.09		978.32			
984.79	96	989.73	97.11	993.	89 98	1002.24	98.9	1002.6	98.98		
Manning's	n Value	:S	กนส=	3							
Sta	n Val	Sta	n Val	S	ta n Val						
8	.07	173.81	.033	793.	47 .05						
Bank Sta:	Left	Right	Leneths	: Lef	t Channel	Right	Coeff	Contr.	Expan.		
	73.81 7	_	20118	316.		316.8		.1	,3		
	J.U	33147		0201	3 320.4	520.0		• ••			
CDOCC CCC	TOU 011	DILT Dag	£\$10 #10								
CROSS SECT	I TON OOI	POI Pro	TITE #10	λı.							
				_	#1				Phase 1	ni-Le co	
E.G. Ele			83.3		Element			eft OB	Channel	Right OB	
Vel Head			0.4		Wt. n-Val.			0.070	0.033	0.050	
W.S. Ele	v (ft)		82.93	3	Reach Len.	(ft)	3	16.30	316.40	316.80	
Crit W.S					Flow Area	(sq ft)	10	14.84	33407.21	910.20	
E.G. Slo		ft)	0.000073		Area (sq f		10	14.84	33407.21	910.20	
Q Total			182000.0		Flow (cfs			023.41	179978.50	998.03	
Top Widt			791.4		Top Width			73.49	619.66	98.27	
Vel Tota		· <b>\</b>	5.1		Avg. Vel.	1 - 7		1.61	5.39	1.10	
			57.7					13.81	53.91	9.26	
Max Chl		_ 1			Hydr. Depti						
Conv. To			21274086		Conv. (ci			19627.1			
Length W		:)	316.40		Wetted Per			77.55	638.74	101.62	
Min Ch E	ii (ft)		25.20		Shear (lb/s			0.06	0.24	0.04	
Alpha			1.0	8	Stream Powe	er (1b/ft		0.06	1.29	0.04	
Frctn Lo	oss (ft)		0.0	2	Cum Volume	(acre-ft)	)	22.54	1356.00	26.61	
C & E Lo	ss (ft)		0.00	0	Cum SA (acı	res)		2.04	25.32	2.76	
CROSS SECT	FTON OUT	PHT Pro	file #50	vr							
CROSS SECT	TION OUT	PUT Pro	file #50	yr							
		PUT Pro		•	Elomon+			aft AR	Channal	Dight OR	
E.G. Ele	v (ft)	PUT Pro	91.5	5	Element			eft OB	Channel	Right OB	
E.G. Ele Vel Head	ev (ft) I (ft)	FPUT Pro	91,59 0.6	5 7	Wt. n-Val.	( <b>5</b> 4 )		0.070	0.033	0.050	
E.G. Ele Vel Head W.S. Ele	ev (ft) I (ft) ev (ft)	FPUT Pro	91.5	5 7 8	Wt. n-Val. Reach Len.		3	0.070 16.30	0.033 316.40	0.050 316.80	
E.G. Ele Vel Head W.S. Ele Crit W.S	ev (ft) I (ft) ev (ft) S. (ft)		91.59 0.67 90.88	5 7 8	Wt. n-Val. Reach Len. Flow Area	(sq ft)	3 16	0.070 16.30 74.87	0.033 316.40 38329.87	0.050 316.80 2042.91	
E.G. Ele Vel Head W.S. Ele	ev (ft) I (ft) ev (ft) S. (ft)		91,59 0.6	5 7 8	Wt. n-Val. Reach Len.	(sq ft)	3 16	0.070 16.30	0.033 316.40	0.050 316.80	
E.G. Ele Vel Head W.S. Ele Crit W.S	ev (ft) d (ft) ev (ft) S. (ft) ope (ft/		91.59 0.67 90.88	5 7 8	Wt. n-Val. Reach Len. Flow Area	(sq ft) t)	3 16 16	0.070 16.30 74.87	0.033 316.40 38329.87 38329.87 254673.70	0.050 316.80 2042.91	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slo	ev (ft) I (ft) ev (ft) S. (ft) ope (ft) (cfs)		91.5 0.6 90.8 0.00009	5 7 8 3	Wt. n-Val. Reach Len. Flow Area Area (sq f	(sq ft) t) )	3 16 16 2	0.070 16.30 74.87 74.87	0.033 316.40 38329.87 38329.87	0.050 316.80 2042.91 2042.91	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slo Q Total Top Widt	ev (ft) I (ft) ev (ft) S. (ft) ope (ft) (cfs) th (ft)	íft)	91.55 0.65 90.86 0.00009 260000.0	5 7 8 3 00 6	Wt. n-Val. Reach Len. Flow Area Area (sq f Flow (cfs	(sq ft) t) ) (ft)	3 16 16 2	0.070 16.30 74.87 74.87 266.08	0.033 316.40 38329.87 38329.87 254673.70	0.050 316.80 2042.91 2042.91 3060.27	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slo Q Total Top Widt Vel Tota	ev (ft) i (ft) ev (ft) s. (ft) ope (ft) (cfs) th (ft)	(ft)	91.5 0.6 90.8 0.00009 260000.1 878.8 6.1	5 7 8 3 00 6 8	wt. n-Val. Reach Len. Flow Area Area (sq fi Flow (cfs Top Width Avg. Vel.	(sq ft) t) ) (ft) (ft/s)	3 16 16 2	0.070 16.30 74.87 74.87 266.08 92.67	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64	0,050 316.80 2042.91 2042.91 3060.27 165.53 1.50	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slo Q Total Top Widt Vel Tota Max Chl	ev (ft) i (ft) ev (ft) s. (ft) ope (ft) (cfs) th (ft) opth (f	(ft) 5) 5t)	91.5 90.6 90.8 0.00009 260000. 878.8 6.1 65.6	5 7 8 3 90 6 8	Wt. n-Val. Reach Len. Flow Area Area (sq f Flow (cfs Top Width Avg. Vel. Hydr. Dept	(sq ft) t) ) (ft) (ft/s) h (ft)	3 16 16 2	0.070 16.30 74.87 74.87 266.08 92.67 1.35 18.07	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slo Q Total Top Widt Vel Tota Max Chl Conv. To	ev (ft) i (ft) ev (ft) s. (ft) ope (ft) (cfs) th (ft) opth (ft)	(ft) (ft) (ft) (fs)	91.5 90.6 90.8 0.00009 260000. 878.8 6.1 65.6 2700752	5 7 8 3 900 6 8 8	Wt. n-Val. Reach Len. Flow Area Area (sq fi Flow (cfs Top Width Avg. Vel. Hydr. Depti	(sq ft) t) ) (ft) (ft/s) h (ft) fs)	3 16 16 2	0.070 16.30 74.87 74.87 266.08 92.67 1.35 18.07 35388.7	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86 26454240.	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slo Q Total Top Widd Vel Tota Max Chl Conv. To Length W	ev (ft) i (ft) ev (ft) c (ft) ope (ft) th (ft) al (ft/s opth (f	(ft) (ft) (ft) (fs)	91.55 0.66 90.86 0.00009 260000.0 878.86 6.11 65.66 27007526 316.46	5 7 8 3 90 6 8 8 8	Wt. n-Val. Reach Len. Flow Area Area (sq fi Flow (cfs Top Width Avg. Vel. Hydr. Deptl Conv. (c	(sq ft) t) ) (ft) (ft/s) h (ft) fs) . (ft)	3 16 16 2	9.070 16.30 74.87 74.87 266.08 92.67 1.35 18.07 35388.7 98.31	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86 26454240.	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2 170.51	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slo Q Total Top Widt Vel Tota Max Chl Conv. To Length W	ev (ft) i (ft) ev (ft) c (ft) ope (ft) th (ft) al (ft/s opth (f	(ft) (ft) (ft) (fs)	91.5: 90.8: 90.8: 0.00009: 260000. 878.8: 6.1: 65.6: 2700752: 316.4: 25.20	5 7 8 3 90 6 8 8 8 9.0	Wt. n-Val. Reach Len. Flow Area Area (sq f' Flow (cfs Tlow Width Avg. Vel. Hydr. Deptl Conv. (c Wetted Per. Shear (lb/s	(sq ft) t) ) (ft) (ft/s) h (ft) fs) . (ft) sq ft)	3 16 16 2 2	0.070 16.30 74.87 74.87 266.08 92.67 1.35 18.07 35388.7 98.31 0.10	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86 26454240. 638.74 0.35	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2 170.51 0.07	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slc Q Total Top Widt Vel Tota Max Chl Conv. To Length W Min Ch Alpha	ev (ft) i (ft) v (ft) c. (ft) ppe (ft) th (ft) th (ft) Dpth (ft) th (ft) th (ft) th (ft)	(ft) 5) 6t) 6s) :)	91.5: 0.6 90.8i 0.00009: 260000. 878.8i 6.1: 65.6i 2700752: 316.4i 25.2i	5 7 8 3 99 6 8 8 8 9,0	Wt. n-Val. Reach Len. Flow Area (sq fi Flow (cfs Top Width Avg. Vel. Hydr. Depti Conv. (cr Shear (lb/s Stream Powe	(sq ft) t) (ft) (ft/s) h (ft) fs) . (ft) sq ft) er (lb/ft	3 16 16 2 2 2	0.070 16.30 74.87 74.87 266.08 92.67 1.35 18.07 35388.7 98.31 0.10	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86 26454240. 638.74 0.35 2.31	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2 170.51 0.07 0.10	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slc Q Total Top Widt Vel Tota Max Chl Conv. To Length W Min Ch E Alpha Frctn Lc	ev (ft) i (ft) ev (ft) sev (ft) ope (ft,	(ft) 5) 5t) 5s)	91.5: 0.6: 90.8: 0.00009: 260000. 878.8: 65.6: 2700752: 316.44: 25.2( 1.1: 0.0:	5 7 8 3 99 6 8 8 8 9,0 9	Wt. n-Val. Reach Len. Flow Area Area (sq ff Flow (cfs Top Width Avg. Vel. Hydr. Deptl Conv. (c: Wetted Per. Shear (lb/: Stream Pow Cum Volume	(sq ft) t) ) (ft) (ft/s) hft) fs) . (ft) sq ft) er (lb/ft (acre-ft)	3 16 16 2 2 2	0.070 16.30 74.87 74.87 266.08 92.67 1.35 18.07 35388.7 98.31 0.10 0.13 41.73	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86 26454240. 638.74 0.35 2.31	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2 170.51 0.07 0.10 53.86	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slc Q Total Top Widt Vel Tota Max Chl Conv. To Length W Min Ch Alpha	ev (ft) i (ft) ev (ft) sev (ft) ope (ft,	(ft) 5) 5t) 5s)	91.5: 0.6 90.8i 0.00009: 260000. 878.8i 6.1: 65.6i 2700752: 316.4i 25.2i	5 7 8 3 99 6 8 8 8 9,0 9	Wt. n-Val. Reach Len. Flow Area (sq fi Flow (cfs Top Width Avg. Vel. Hydr. Depti Conv. (cr Shear (lb/s Stream Powe	(sq ft) t) ) (ft) (ft/s) hft) fs) . (ft) sq ft) er (lb/ft (acre-ft)	3 16 16 2 2 2	0.070 16.30 74.87 74.87 266.08 92.67 1.35 18.07 35388.7 98.31 0.10	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86 26454240. 638.74 0.35 2.31	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2 170.51 0.07 0.10	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slc Q Total Top Widt Vel Tota Max Chl Conv. To Length W Min Ch E Alpha Frctn Lc	ev (ft) i (ft) ev (ft) sev (ft) ope (ft,	(ft) 5) 5t) 5s)	91.5: 0.6: 90.8: 0.00009: 260000. 878.8: 65.6: 2700752: 316.44: 25.2( 1.1: 0.0:	5 7 8 3 99 6 8 8 8 9,0 9	Wt. n-Val. Reach Len. Flow Area Area (sq ff Flow (cfs Top Width Avg. Vel. Hydr. Deptl Conv. (c: Wetted Per. Shear (lb/: Stream Pow Cum Volume	(sq ft) t) ) (ft) (ft/s) hft) fs) . (ft) sq ft) er (lb/ft (acre-ft)	3 16 16 2 2 2	0.070 16.30 74.87 74.87 266.08 92.67 1.35 18.07 35388.7 98.31 0.10 0.13 41.73	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86 26454240. 638.74 0.35 2.31	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2 170.51 0.07 0.10 53.86	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slc Q Total Top Widt Vel Tota Max Chl Conv. To Length W Min Ch E Alpha Frctn Lc	ev (ft) i (ft) ev (ft) sev (ft) ope (ft,	(ft) 5) 5t) 5s)	91.5: 0.6: 90.8: 0.00009: 260000. 878.8: 65.6: 2700752: 316.44: 25.2( 1.1: 0.0:	5 7 8 3 99 6 8 8 8 9,0 9	Wt. n-Val. Reach Len. Flow Area Area (sq ff Flow (cfs Top Width Avg. Vel. Hydr. Deptl Conv. (c: Wetted Per. Shear (lb/: Stream Pow Cum Volume	(sq ft) t) ) (ft) (ft/s) hft) fs) . (ft) sq ft) er (lb/ft (acre-ft)	3 16 16 2 2 2	0.070 16.30 74.87 74.87 266.08 92.67 1.35 18.07 35388.7 98.31 0.10 0.13 41.73	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86 26454240. 638.74 0.35 2.31	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2 170.51 0.07 0.10 53.86	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slc Q Total Top Widt Vel Tota Max Chl Conv. To Length W Min Ch E Alpha Frctn Lc	ev (ft) I (ft) S. (ft) S. (ft) DPE (ft/ (cfs) th (ft) al (ft/s DPH (f DHH (f DH (f DHH	(ft) (ft) (ft) (ft) (ft) (ft)	91.5: 90.6: 90.8: 0.00009: 260000. 878.8: 65.6: 2700752: 316.4: 25.2: 1.1: 9.0: 0.00	5 7 8 3 90 6 8 8 8 8 0 0 0 0	Wt. n-Val. Reach Len. Flow Area Area (sq ff Flow (cfs Top Width Avg. Vel. Hydr. Deptl Conv. (c: Wetted Per. Shear (lb/: Stream Pow Cum Volume	(sq ft) t) ) (ft) (ft/s) hft) fs) . (ft) sq ft) er (lb/ft (acre-ft)	3 16 16 2 2 2	0.070 16.30 74.87 74.87 266.08 92.67 1.35 18.07 35388.7 98.31 0.10 0.13 41.73	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86 26454240. 638.74 0.35 2.31	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2 170.51 0.07 0.10 53.86	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slo Q Total Top Widt Vel Tota Max Chl Conv. To Length W Min Ch E Alpha Frctn Lo C & E Lo	ev (ft) I (ft) S. (ft) S. (ft) DPE (ft/ (cfs) th (ft) al (ft/s DPH (f DHH (f DH (f DHH	(ft) (ft) (ft) (ft) (ft) (ft)	91.5: 90.6: 90.8: 0.00009: 260000. 878.8: 65.6: 2700752: 316.4: 25.2: 1.1: 9.0: 0.00	5 7 8 3 90 6 8 8 8 8 0 0 0 0	Wt. n-Val. Reach Len. Flow Area Area (sq ff Flow (cfs Top Width Avg. Vel. Hydr. Deptl Conv. (c: Wetted Per. Shear (lb/: Stream Pow Cum Volume	(sq ft) t) ) (ft) (ft/s) hft) fs) . (ft) sq ft) er (lb/ft (acre-ft)	3 16 16 2 2 2	0.070 16.30 74.87 74.87 266.08 92.67 1.35 18.07 35388.7 98.31 0.10 0.13 41.73	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86 26454240. 638.74 0.35 2.31	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2 170.51 0.07 0.10 53.86	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slo Q Total Top Widt Vel Tota Max Chl Conv. To Length W Min Ch Alpha Frctn Lo C & E Lo CROSS SECT	ev (ft) i (ft) ev (ft) ev (ft) ev (ft) ppe (ft,	(ft) (ft) (ft) (ft) (ft) (ft)	91.5: 0.6: 90.8: 0.00009: 260000.( 878.8: 65.6: 2700752: 316.4( 25.2: 1.1: 0.0: 0.0:	5 7 8 3 99 6 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9	Wt. n-Val. Reach Len. Flow Area Flow (cfs Flow (cfs Top Width Avg. Vel. Hydr. Depti Conv. (c Wetted Per Shear (lb/ Stream Pow Cum Volume Cum SA (aci	(sq ft) t) ) (ft) (ft/s) hft) fs) . (ft) sq ft) er (lb/ft (acre-ft)	3 16 16 2 2 2 s)	0.070 16.30 74.87 266.08 92.67 1.35 18.07 35388.7 98.31 0.10 0.13 41.73 2.82	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86 26454240, 638.74 0.35 2.31 1556.56 25.32	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2 170.51 0.07 0.10 53.86 3.98	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slc Q Total Top Widt Vel Tota Max Chl Conv. To Length W Min Ch E Alpha Frctn Lc C & E Lc CROSS SECT	ev (ft) i (ft) ev (ft) sev (ft) ope (ft,	(ft) (ft) (ft) (ft) (ft) (ft)	91.5: 0.6: 90.8: 0.00009: 260000. 878.8: 65.6: 2700752: 316.4: 25.2: 1.1: 0.0: 0.0:	5 7 8 3 90 6 8 8 8 8 9 0 9 9 9 9 9 9 9 9	Wt. n-Val. Reach Len. Flow Area Area (sq fr Flow (cfs Top Width Avg. Vel. Hydr. Deptl Conv. (c Wetted Per. Shear (lb/: Stream Pow Cum Volume Cum SA (aci	(sq ft) t) ) (ft) (ft/s) hft) fs) . (ft) sq ft) er (lb/ft (acre-ft)	3 16 16 2 2 2 s)	0.070 16.30 74.87 74.87 266.08 92.67 1.35 18.07 35388.7 98.31 0.10 0.13 41.73 2.82	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86 26454240. 638.74 0.35 2.31 1556.56 25.32	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2 170.51 0.07 0.10 53.86 3.98	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slc Q Total Top Widt Vel Tota Max Chl Conv. To Length W Min Ch E Alpha Frctn Lc C & E Lc CROSS SECT E.G. Ele Vel Head	ev (ft) i (ft) ev (ft) sev (ft) ope (ft/ (cfs) th (ft) al (ft/s Dpth (f otal (cf vtd. (ft ) Doss (ft)  FION OUT  Ev (ft) of (ft)	(ft) (ft) (ft) (ft) (ft) (ft)	91.5: 0.6: 90.8: 0.00009: 260000. 878.8: 65.6: 2700752: 316.4: 25.2: 1.1: 0.0: 0.0:	5 7 8 3 90 6 6 8 8 8 8 8 9 0 9 0 9 0 0 0 0 0 0 0 0 0 0	Wt. n-Val. Reach Len. Flow Area Area (sq ff Flow (cfs Top Width Avg. Vel. Hydr. Deptl Conv. (c Wetted Per Stream Pow Cum SA (ac)	(sq ft) t) ) (ft) (ft/s) h (ft) fs) . (ft) sq ft) er (1b/ft (acre-ft) res)	3 16 16 2 2 2 s)	0.070 16.30 74.87 74.87 74.87 13.5 18.07 35388.7 98.31 0.10 0.13 41.73 2.82 eft OB 0.070	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86 26454240. 638.74 0.35 2.31 1556.56 25.32	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2 170.51 0.07 0.10 53.86 3.98	
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E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slo Q Total Top Widt Vel Tota Max Chl Conv. To Length W Min Ch E Alpha Frctn Lc C & E Lc CROSS SECT E.G. Ele Vel Head W.S. Ele Crit W.S	ev (ft) I (ft) I (ft) S. (ft) S. (ft) Ope (ft/ Cofs) Ch (ft/s Dpth (ft/ Cotal (ft) Coss (ft)	(ft) (ft) (ft) (fs) (fs) (fr) (fr) (fr) (fr) (fr) (fr) (fr) (fr	91.5: 90.6: 90.8: 0.00009: 260000. 878.8: 65.6: 2700752: 316.4: 25.2: 1.1: 0.0: 0.0: 0.0: 0.0: 95.1: 0.8: 94.3:	5 7 8 3 900 6 8 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	Wt. n-Val. Reach Len. Flow Area Area (sq ff Flow (cfs Top Width Avg. Vel. Hydr. Deptl Conv. (c Wetted Per Shear (lb/s Stream Powe Cum SA (aci	(sq ft) t) ) (ft) (ft/s) h (ft) fs) . (ft) sq ft) er (lb/ft (acre-ft) res)  (ft) (sq ft) (sq ft)	3 16 16 2 2 s)	0.070 16.30 74.87 74.87 266.08 92.67 1.35 18.07 35388.7 98.31 0.10 0.13 41.73 2.82 eft OB 0.670 06.30 06.72	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86 26454240. 638.74 0.35 2.31 1556.56 25.32 Channel 0.033 316.40 40453.96	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2 170.51 0.07 0.10 53.86 3.98 Right OB 0.050 316.80 2642.55	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. SIG Q Total Top Widt Vel Tota Max Chl Conv. To Length W Min Ch E Alpha Frctn Lc C & E Lc CROSS SECT E.G. Ele Vel Head W.S. Ele Crit W.S E.G. SIG	ev (ft)  I (ft)	(ft) (ft) (ft) (fs) (fs) (fr) (fr) (fr) (fr) (fr) (fr) (fr) (fr	91.5: 0.6: 90.8: 0.00009: 260000.: 878.8: 6.1: 65.6: 2700752: 316.4: 25.2: 1.1: 0.0: 0.0: 95.1: 0.8: 94.3: 0.00010.	5 7 8 3 9 9 6 8 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9	Wt. n-Val. Reach Len. Flow Area (sq fi Flow (cfs Top Width Avg. Vel. Hydr. Depti Conv. (cr Wetted Per Shear (lb/: Stream Pow Cum Volume Cum SA (aci Element Wt. n-Val. Reach Len. Flow Area Area (sq fi	(sq ft) t) ) (ft) (ft/s) h (ft) fs) . (ft) sq ft) er (lb/ft (acre-ft) res)  (ft) (sq ft) t)	3 16 16 2 2 3 20 20 20	0.070 16.30 74.87 74.87 266.08 92.67 1.35 18.07 35388.7 98.11 0.13 41.73 2.82 eft OB 0.070 16.30 06.72	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86 26454240. 638.74 0.35 2.31 1556.56 25.32 Channel 0.033 316.40 40453.96	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2 170.51 0.07 0.10 53.86 3.98  Right OB 0.050 316.80 2642.55	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slc Q Total Top Widt Vel Tota Max Chl Conv. To Length W Min Ch E Alpha Frctn Lo C & E Lo  CROSS SECT E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slc Q Total	ev (ft) i (ft) ev (ft) ev (ft) ppe (ft, (cfs) th (ft) il (ft/s) Dpth (ft) th (ft) il (ft) il (ft) ivtd. (ft) il (ft) ivtd. (ft) ivtd	(ft) (ft) (ft) (fs) (fs) (fr) (fr) (fr) (fr) (fr) (fr) (fr) (fr	91.5: 0.6 90.8i 0.00009: 260000.i 878.8i 65.6i 2700752: 316.4i 25.2i 0.0: 0.0: file #100 95.1: 0.8i 94.3i 0.00010.302000.i	5 7 8 3 90 6 8 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	Wt. n-Val. Reach Len. Flow Area Area (sq fi Flow (cfs Top Width Avg. Vel. Hydr. Depti Conv. (c: Wetted Per. Shear (lb/: Stream Powc Cum Volume Cum SA (aci Element Wt. n-Val. Flow Area Area (sq fi Flow (cfs	(sq ft) t) ) (ft) (ft/s) h (ft) fs) . (ft) sq ft) er (lb/ft (acre-ft) res)  (ft) (sq ft) t) )	3 166 166 2 2 s)	0.070 16.30 74.87 74.87 72.66.08 92.67 1.35 18.07 35388.7 98.31 0.10 0.13 41.73 2.82 eft OB 0.070 16.30 06.72 06.72	0.033 316.40 38329.87 254673.70 619.66 6.64 61.86 26454240. 638.74 0.35 2.31 1556.56 25.32 Channel 0.033 316.40 40453.96 40453.96 294286.70	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2 170.51 0.07 0.10 53.86 3.98  Right OB 0.050 316.80 2642.55 2642.55	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slc Q Total Top Widt Vel Tota Max Chl Conv. To Length W Min Ch Alpha Frctn Lc C & E Lc CROSS SECT E.G. Ele Vel Head W.S. Ele Crit W.S. Ele Crit Slc Q Total Top Widt	ev (ft) i (ft) ev (ft) pev (ft) ppe (ft) (cfs) th (ft) el (ft) il (ft) sss (ft) cv (ft) sss (ft) ev (ft) ss (ft) ev (ft) cofs) th (ft) ev (ft) cofs) th (ft)	(ft) s) ft) fs) rPUT Pro	91.5: 0.6 90.8i 0.00009: 260000.i 878.8i 65.6i 2700752i 316.4i 25.2i 0.0: 0.0: file #10i 95.1: 0.8i 94.3i 0.00010. 302000.i 903.6i	5 7 8 3 90 6 6 8 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9	Wt. n-Val. Reach Len. Flow Area Area (sq ff Flow (cfs Top Width Avg. Vel. Hydr. Deptl Conv. (cr Wetted Per. Shear (lb/: Stream Powc Cum Volume Cum SA (aci Element Wt. n-Val. Reach Len. Flow Area Area (sq ff Flow (cfs Top Width	(sq ft) t) ) (ft) (ft/s) h (ft) fs) . (ft) er (1b/ft) res)  (ft) (sq ft) t) (sq ft) t) (sq ft)	3 166 166 2 2 s)	0.070 16.30 74.87 74.87 74.87 135 18.07 35388.7 98.31 0.10 0.13 41.73 2.82 eft OB 0.070 16.30 06.72 06.72	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86 26454240. 638.74 0.35 2.31 1556.56 25.32 Channel 0.033 316.40 40453.96 40453.96 294286.70 619.66	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2 170.51 0.07 0.10 53.86 3.98  Right OB 0.050 316.80 2642.55 2642.55 4661.15 183.04	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slc Q Total Top Widt Vel Tota Max Chl Conv. To Length W Min Ch E Alpha Frctn Lo C & E Lo  CROSS SECT E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slc Q Total	ev (ft) i (ft) ev (ft) pev (ft) ppe (ft) (cfs) th (ft) el (ft) il (ft) sss (ft) cv (ft) sss (ft) ev (ft) ss (ft) ev (ft) cofs) th (ft) ev (ft) cofs) th (ft)	(ft) s) ft) fs) rPUT Pro	91.5: 0.6 90.8i 0.00009: 260000.i 878.8i 65.6i 2700752: 316.4i 25.2i 0.0: 0.0: file #100 95.1: 0.8i 94.3i 0.00010.302000.i	578830068880000100000000000000000000000000	Wt. n-Val. Reach Len. Flow Area Area (sq ff Flow (cfs Top Width Avg. Vel. Hydr. Deptl Conv. (c Wetted Per. Shear (lb/: Stream Pow Cum Volume Cum SA (acm Element Wt. n-Val. Reach Len. Flow Area (sq ff Flow (cfs Top Width Avg. Vel.	(sq ft) t) ) (ft) (ft/s) h (ft) fs) . (ft) sq ft) er (1b/ft (acre-ft) res)  (ft) (sq ft) t) ) (ft) (ft) (ft/s)	3 16 16 2 2 (s)	0.070 16.30 74.87 74.87 74.87 13.5 18.07 35388.7 98.31 0.10 0.13 41.73 2.82 eft OB 0.070 16.30 06.72 065.72 052.14	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86 26454240. 638.74 0.35 2.31 1556.56 25.32 Channel 0.033 316.40 40453.96 40453.96 294286.70 619.66 7.27	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2 170.51 0.07 0.10 53.86 3.98  Right OB 0.050 316.80 2642.55 2642.55 4661.15 183.04 1.76	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slc Q Total Top Widt Vel Tota Max Chl Conv. To Length W Min Ch Alpha Frctn Lc C & E Lc CROSS SECT E.G. Ele Vel Head W.S. Ele Crit W.S. Ele Crit Slc Q Total Top Widt	ev (ft)  I (ft)  ev (ft)  pev (ft)  poe (ft/  (cfs)  th (ft/s)  Doth (ft)  th (ft)  std (ft)  coss	/ft) s) ft) fs) rPUT Pro /ft)	91.5: 0.6 90.8i 0.00009: 260000.i 878.8i 65.6i 2700752i 316.4i 25.2i 0.0: 0.0: file #10i 95.1: 0.8i 94.3i 0.00010. 302000.i 903.6i	57883006888000000000000000000000000000000	Wt. n-Val. Reach Len. Flow Area Area (sq ff Flow (cfs Top Width Avg. Vel. Hydr. Deptl Conv. (cr Wetted Per. Shear (lb/: Stream Powc Cum Volume Cum SA (aci Element Wt. n-Val. Reach Len. Flow Area Area (sq ff Flow (cfs Top Width	(sq ft) t) ) (ft) (ft/s) h (ft) fs) . (ft) sq ft) er (1b/ft (acre-ft) res)  (ft) (sq ft) t) ) (ft) (ft) (ft/s)	3 16 16 2 2 (s)	0.070 16.30 74.87 74.87 74.87 135 18.07 35388.7 98.31 0.10 0.13 41.73 2.82 eft OB 0.070 16.30 06.72 06.72	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86 26454240. 638.74 0.35 2.31 1556.56 25.32 Channel 0.033 316.40 40453.96 40453.96 294286.70 619.66	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2 170.51 0.07 0.10 53.86 3.98  Right OB 0.050 316.80 2642.55 2642.55 4661.15 183.04	
E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slc Q Total Top Widt Vel Tota Max Chl Conv. To Length W Min Ch E Alpha Frctn Lc C & E Lc  CROSS SECT  E.G. Ele Vel Head W.S. Ele Crit W.S E.G. Slc Q Total Top Widt Vel Tota	ev (ft)  I (ft)  ev (ft)  pev (ft)  poe (ft/  (cfs)  th (ft/s)  Doth (ft)  th (ft)  std (ft)  coss	/ft) s) ft) fs) rPUT Pro /ft)	91.5: 90.8: 90.8: 0.00009: 260000.6 878.8: 65.1: 65.6: 2700752: 316.4: 25.2: 1.1: 0.0: 0.0: 9.8: 94.3: 0.00010: 302000.6 903.6:	57883006888000000000000000000000000000000	Wt. n-Val. Reach Len. Flow Area Area (sq ff Flow (cfs Top Width Avg. Vel. Hydr. Deptl Conv. (c Wetted Per. Shear (lb/: Stream Pow Cum Volume Cum SA (acm Element Wt. n-Val. Reach Len. Flow Area (sq ff Flow (cfs Top Width Avg. Vel.	(sq ft) t) ) (ft) (ft/s) h (ft) fs) . (ft) sq ft) er (1b/ft (acre-ft) res)  (ft) (sq ft) t) ) (ft) (ft) (ft/s)	3 16 16 2 2 (s)	0.070 16.30 74.87 74.87 74.87 13.5 18.07 35388.7 98.31 0.10 0.13 41.73 2.82 eft OB 0.070 16.30 06.72 065.72 052.14	0.033 316.40 38329.87 38329.87 254673.70 619.66 6.64 61.86 26454240. 638.74 0.35 2.31 1556.56 25.32 Channel 0.033 316.40 40453.96 40453.96 294286.70 619.66 7.27	0.050 316.80 2042.91 2042.91 3060.27 166.53 1.50 12.27 0 317886.2 170.51 0.07 0.10 53.86 3.98  Right OB 0.050 316.80 2642.55 2642.55 4661.15 183.04 1.76	

Length Min Ch Alpha Frctn L	otal (control (contro	t) )	2970101 316.4 25.2 1.1 0.0	1 Wet 0 She 5 Str 4 Cum		(ft) q ft) r (lb/ft (acre-ft)	s)	800170.5 107.28 0.12 0.18 51.94 3.17	28942420.6 638.74 0.41 2.97 1642.98 25.32	458413.2 187.37 0.09 0.16 68.28 4.48
CROSS SEC	TION									
RIVER: Wi REACH: Bu			RS: 42.	93						
INPUT Descripti	on: Ups	tream Fac	e of Doc							
Station E	levation	n Data	กบส=	73						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	104.14	4.34	103.73	22,37	102	23.41	102	29.9	101.36	
30.63	101.32		100	53.06	99.14	62.22	98	63.11	98	
63.66	97.63		96	71.06	94	75.13	92		96	
83.27	88		86	87.82	85.77	90.85	84		82	
97.6		101.05		104.51	76	107.98	74		72	
							64		62.35	
114.9	70		69.98	121.01	66	124.06	26.52		25.3	
127.81		128.85	61.47	131.25	60	170				
414.3	25.1		25.1	680	26.15	703.68	43.38		46.47	
735.26	47.34			750.05		760.64	57.56		59.8	
763.63	69			777.55		785.38		786.02		
796.82	71.4	806.08	74.49	810.33	75.46		76.78			
834.82	79.7	840.199	81,11	847.62	82.71	859.14	84.92	864.18	85.61	
880.6	89.7	885.18	90.96	898.11	94	911.16	95	923.22	98	
937.25	100	945.28	102	948.35	102.11	970.48	102.44	971.36	102.39	
978.01	102	998.15	102	999.16	102					
Manning's	n Valu	es	กนต=	3						
Sta	n Val		n Val	Sta	n Val					
0	.07			763.63	.05					
·				, , , , , ,	,,,,					
Bank Sta:	Laft	Right	Lengths	; Left (	hannel	Right	Coef	f Contr.	Expan.	
		763.63	rengens	1404	1426	1448		.1	.3	
Blocked 0			Must-	1	1420	1440		• • •	.5	
			num⇒	1						
Sta L	Sta R	Elev								
703.5	704.5	100								
CROSS SEC	TION OU	TPUT Pro	)+11e #10	yr						
_										
E.G. El	ev (ft)		83.3		ement			Left OB	Channel	Right OB
Vel Hea	d (ft)		0.4	4 Wt.	n-Val.			0.070	0.033	0.050
W.S. El	ev (ft)		82.9	1 Rea	ich Len.	(ft)	14	404.00	1426.00	1448.00
Crit W.	S. (ft)			F10	ow Area (	(sq ft)		439.47	33957.44	768.41
E.G. 51	ope (ft	/ft)	0.00008	4 Are	ea (sq ft	:)		439.47	33957.44	768.41
Q Total			182000.	00 F	low (cfs)	ı İ		390.96	180744.40	864.63
	th (ft)		754.9		width (			38.53	631.38	85,05
	al (ft/		5.1		, Vel.	: - '		0.89	5,32	1,13
	Dpth (	•	57.8	_	ir. Depti			11.41	53.78	9.04
	otal (c		1988390		conv. (ci			42713.7	19746720.0	
					tted Per	*		44.85	731.67	91.33
	Wtd. (f	-	1426.0						0.24	
	El (ft)		25.1		ear (lb/s		۵١.	9.05		0.04
Alpha			1.0			er (lb/ft		0.05	1,29	0.05
	oss (ft	:	0.1			(acre-ft	,	17.26	1111.35	20.51
C & E L	oss (ft	)	0.0	₩ Cur	n SA (acı	res)		1.63	20.77	2.09
Warning:	Divided	flow con	nputed fo	r this o	ross-sec	tion.				

CROSS SECTION OUTPUT Profile #50 yr

E.G. Elev (ft) Vel Head (ft) 91.51 Element 0.66 Wt. n-Val. Left OB 0.070 Channel Right OB 0.033 0.050

W.S. Elev (ft)	90.85	Reach Len. (ft)	1404.00	1426.00	1448.00
Crit W.S. (ft)		Flow Area (sq ft)	803.51	38968.83	1599.01
E.G. Slope (ft/ft)	0.000110	Area (sq ft)	803.51	38968.83	1599.01
Q Total (cfs)	260000.00	Flow (cfs)	984.59	256341.60	2673.78
Top Width (ft)	806.31	Top Width (ft)	53.78	631.38	121.15
Vel Total (ft/s)	6.28	Avg. Vel. (ft/s)	1.23	6.58	1.67
Max Chl Doth (ft)	65.75	Hydr. Depth (ft)	14,94	61.72	13.20
Conv. Total (cfs)	24835460.0	Conv. (cfs)	94049.4	24486010.6	255402.5
Length Wtd. (ft)	1426.97	Wetted Per. (ft)	62.06	747.55	128.33
Min Ch El (ft)	25.10	Shear (lb/sq ft)	0.09	0.36	0.09
Alpha	1.08	Stream Power (lb/ft s)	0.11	2.35	0.14
Fretn Loss (ft)	0.14	Cum Volume (acre-ft)	32.73	1275.83	40.62
C & E Loss (ft)	0.00	Cum SA (acres)	2.29	20.77	2,94

Warning: Divided flow computed for this cross-section.

CROSS SECTION OUTPUT Profile #100 yr

E.G. Elev (ft)	95.07	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.80	Wt. n-Val.	0.070	0.033	0.050
W.S. Elev (ft)	94.27	Reach Len. (ft)	1404.00	1426.00	1448.00
Crit W.S. (ft)		Flow Area (sq ft)	999.50	41129.89	2038.45
E.G. Slope (ft/ft)	0.000124	Area (sq ft)	999.50	41129.89	2038,45
Q Total (cfs)	302000.00	flow (cfs)	1393,59	296654.00	3952.45
Top Width (ft)	828.39	Top Width (ft)	60.75	631.38	136,26
Vel Total (ft/s)	6.84	Avg. Vel. (ft/s)	1.39	7.21	1.94
Max Chl Dpth (ft)	69.17	Hydr, Depth (ft)	16.45	65.14	14.96
Conv. Total (cfs)	27108320.0	Conv. (cfs)	125091.9	26628440.0	354782.2
Length Wtd. (ft)	1426.09	Wetted Per. (ft)	69.82	754.39	143.83
Min Ch El (ft)	25.10	Shear (1b/sq ft)	0.11	0.42	0.11
Alpha	1.09	Stream Power (1b/ft s)	0.15	3.05	0.21
Frctn Loss (ft)	0.16	Cum Volume (acre-ft)	41.03	1346.69	51,25
C & E Loss (ft)	0.00	Cum SA (acres)	2.58	20.77	3.32

Elev

77.81

88

80

74

64

60

Warning: Divided flow computed for this cross-section.

CROSS SECTION

RIVER: Willamette R

REACH: Butteville RS: 42.66

INPUT Description: C section

Station Elevation Data **们业的**= 56 Sta Sta Elev Sta Elev Sta Elev Sta Elev 92 34.8 96 15.33 94 21.82 0 98.73 8.85 60.75 38.86 86 47.78 84 54.26 82 86.75 41.29 77.84 60.82 80 68.07 78.3 68.78 78 69.39 69.51 69.82 77.7 71.07 77.32 75,18 76 75.8 75.79 81.09 72 66 102.82 65.62 106.55 86.94 92.2 70 101.89 61.88 113.92 60.22 114.31 111.01 62.2 111.05 62 111.25 187 29.5 294.3 25.5 414.3 25,1 525,1 25.1 629.2

26 705 29.06 751.96 60 759.12 766.29 68 773.45 72 780.61 76 787.78 80 794.94 84 802.1 88 810.09 92 98 849,12 96 832.03 102 813,49 93.66 814.93 94 823.48 103.4 875.15 103.03 877.1 103.05 881.32 102.91 854.84 103.34 859.57

894.09 102.64

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
0 .07 114.31 .033 751.96 .05

Bank Sta: Left Right Coeff Contr. Expan. 114.31 751.96 .1 .3

CROSS SECTION OUTPUT Profile #10 yr

E.G. Elev (ft)	83.24	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.44	Wt. n-Val.	0.070	0.033	0.050
W.S. Elev (ft)	82.80	Reach Len. (ft)	474 64	****	465 45
Crit W.S. (ft)	41.60	Flow Area (sq ft)	631.26	33939.06	465.47
E.G. Slope (ft/ft)	0.000072	Area (sq ft)	631.26	33939.06	465.47
Q Total (cfs)	182000.00	Flow (cfs)	508.62	180947.10	544.29
Top Width (ft)	741.12	Top Width (ft)	62.64	637.65	40.83
Vel Total (ft/s)	5.19	Avg. Vel. (ft/s)	0.81	5.33	1.17
Max Chl Dpth (ft)	57.70	Hydr. Depth (ft)	10.08	53.23	11.40
Conv. Total (cfs)	21402630.0	Conv. (cfs)	59812.1		
Length Wtd. (ft)		Wetted Per. (ft)	66.94	653.21	46.77
Min Ch El (ft)	25.10	Shear (1b/sq ft)	0.04	0.23	0.64
Alpha	1.05	Stream Power (1b/ft s)	0.03	1.25	0.05
Fretn Loss (ft)		Cum Volume (acre-ft)			
C & E Loss (ft)		Cum SA (acres)			
CROSS SECTION OUTPUT	Profile #50 yr				
E.G. Elev (ft)	91.37	Element	Left 08	Channel	Right OB
Vel Head (ft)	0.67	Wt. n-Val.	0.070	0.033	0.050
W.S. Elev (ft)	90.70	Reach Len. (ft)			
Crit W.S. (ft)	45.71	Flow Area (sq ft)	1227.34	38976.49	844.66
E.G. Slope (ft/ft)	0.000092	Area (sq ft)	1227.34	38976.49	844.66
Q Total (cfs)	260000.00	Flow (cfs)	1389.15	257257.50	1353.35
Top Width (ft)	781.45	Top Width (ft)	88.27	637.65	55.53
Vel Total (ft/s)	6,33	Avg. Vel. (ft/s)	1.13	6.60	1,60
Max Chl Dpth (ft)	65.60	Hydr. Depth (ft)	13.90	61.13	15.21
Conv. Total (cfs)	27084710.0	Conv. (cfs)	144710,2		
Length Wtd. (ft)	2700112010	Wetted Per. (ft)	93.76	653.21	63.46
Min Ch El (ft)	25.10	Shear (1b/sq ft)	0.08	0.34	0.08
Alpha	1.07	Stream Power (lb/ft s)	0.09	2,27	0.12
Freta Loss (ft)		Cum Volume (acre-ft)			
C & E Loss (ft)		Cum SA (acres)			
CROSS SECTION OUTPUT	Profile #100 yr				
E.G. Elev (ft)	94.91	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.81	Wt. n-Val.	0.070	0.033	0.050
W.S. Elev (ft)	94.10	Reach Len. (ft)			
Crit W.S. (ft)	47.66	Flow Area (sq ft)	1546.22	41144.50	1045.34
E.G. Slope (ft/ft)	0.000103	Area (sq ft)	1546,22	41144.50	1045.34
Q Total (cfs)	302 <del>0</del> 00.00	Flow (cfs)	2000.54	298121.30	1878.14
Top Width (ft)	800.35	Top Width (ft)	99.30	637.65	63.40
Vel Total (ft/s)	6.91	Avg. Vel. (ft/s)	1.29	7.25	1.80
Max Chl Dpth (ft)	69.00	Hydr. Depth (ft)	15.57	64.53	16.49
Conv. Total (cfs)	29710820.0	Conv. (cfs)	196813.8		
Length Wtd. (ft)		Wetted Per. (ft)	105.30	653.21	72.07
Min Ch El (ft)	25.10	Shear (1b/sq ft)	0.09	0.41	0.09
Alpha	1.09	Stream Power (lb/ft s)	0.12	2.94	0.17
Frctn Loss (ft)		Cum Volume (acre-ft)			
C & E Loss (ft)		Cum SA (acres)			

#### SUMMARY OF MANNING'S N VALUES

#### River:Willamette R

Reach	River Sta.	n1	n2	n3
Butteville	43.30	.07	.033	.05
Butteville	42.99	.07	.033	. 05
Butteville	42.93	. 97	.033	.05
Butteville	42.66	. 07	.033	.05

#### SUMMARY OF REACH LENGTHS

River: Willamette R

Reach	River Sta.	Left	Channel	Right
Butteville	43,30	1583.2	1636.8	1756.1
Butteville	42.99	316.3	316.4	316.8
Butteville	42.93	1404	1426	1448
Butteville	42.66			

# SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS River: Willamette $\ensuremath{R}$

Reach	River Sta.	Contr.	Expan	
Butteville	43.30	,1	.3	
Butteville	42.99	.1	.3	
Butteville	42.93	.1	.3	
Butteville	42.66	,1	.3	

#### Profile Output Table - Standard Table 1

Reach Vel Chnl	River Flow Area		Profile th Frouc	Q Total le # Chl	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope
V42 4/11/2	7 2011 711 00	10pu		(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)
(ft/s)	(sq ft)	(ft)		(/	,	<b>(</b> , -,	( ,	( · - /	( · · · · · · · · · · · · · · · · · · ·
									•
Buttevi:	lle 43.30		10 yr	182000,00	7,50	83.01	•	83.55	0.000106
	1649.12	750.54		0.15				****	
Buttevi]	lle 43.30		50 yr	260000.00	7.50	90.97		91.76	0.000126
7.15	37771.12	790.81		0.17					
Buttevi]			100 yr	302000.00	7.50	94.41		95.34	0.000138
7.79	10635.84	895.06		0.18					
Buttevi:	lle 42.99		10 vs	182000.00	25.20	82.93		83,38	0.000073
	35332.25	791,42		0.13	23.20	02.33		03.30	0.000073
Buttevi.			50 yr	250000.00	25,20	90.88		91.55	0.000093
	2047.64	878.86		0.15					
Buttevi)	le 42.99		100 yr	302000.00	25.20	94.30		95.11	0.000103
7.27	15103.23	903.65	•	0.16					
Buttevi]	lle 42.93		10 un	182000.00	25.10	82,91		83.35	0.000084
	35165.31	754.96		0.13	25,10	62,91		65,33	0.000004
Buttevi]			50 vr	250000,00	25.10	90.85		91.51	0.000110
	1371.35	806.31	,	0.15				72132	01000220
Buttevi)			100 yr	302000.00	25.10	94.27		95.07	0.000124
7.21	14167.85	828.39	•	0.16					
- 44 5									
Buttevil			1 <del>0</del> yr	182000.00	25.10	82.80	41.60	83.24	0.000072
5.33 3 Buttevil	35035.79 lle 42.66	741.12		0.13 260000.00	25.10	90.70	45.71	91,37	0.000092
	11048.49	781.45	50 yr	0.15	25.10	90.70	45.71	31.37	0.000092
Buttevi			100 vr	302000.00	25.10	94.10	47.66	94.91	0.000103
	3736.06	800.35	,	0.16	23.20	54.20	47100	34.31	0.000105



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# Conveyance Compensation Cut

# Assumptions:

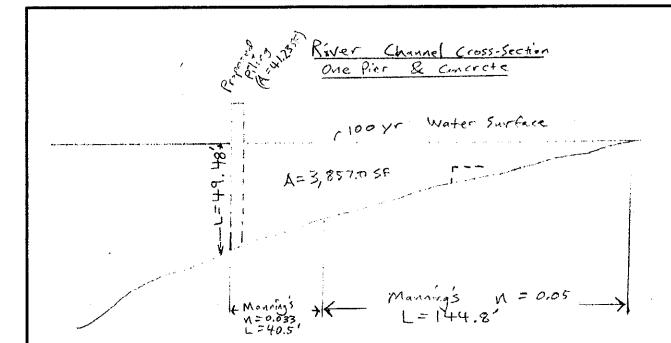
- · Only the Stations Along the Cross-section of the River that the planned dark impacts is all that we are looking at when Calculating the conveyance loss-
- . The worst case cross section on the dock is the one with the pier furthest out along the dock after the angle point. The concrete is not in this cross section.
- · the manning's in coefficient is a roughness number that is used in water flow Calculations and is different for each surface the water flows over the manning's a coefficient for the Channel we defined as station 8+25.2' toward the center. The mannings n for the right bank starts at station 8+25.2' and continues away from the Center line of the Willomette River.
- . The Right of way lines are not perrollel to the cross-section of the River at the dock and the Right of way lines are not perpendicular to the Centerline of the River. RED PROPE

EXPIRES: 12/31/2021

	SDW	Butteville Landing Conveyance & compesation (ut	11/17/21	1/7
Job No.	By	Subject	Date	Sheet No.



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# Pre Construction

$$A = 5689.25F \qquad N = \frac{(0.033) \cdot (82.0) + (0.05) \cdot (144.8')}{226.8}$$

$$NP = 226.8 ft$$
  $N = 0.0439$   $R = 25.08$ 



EXPIRES: 12/31/2021

		Butteville Landing		2/7
	SDW	Conveyance & Compensation Cut	12/1/21	<i></i>
Job No.	Ву	Subject	Date	Sheet No.



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#### **UpStream**

# Post Construction

$$V = \frac{(0.0434)(55(.8) + (0.015) \cdot (44.0)}{352.8}$$

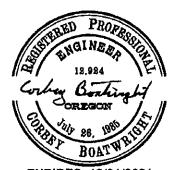
$$R = 17.33$$
 $R^{3/3} = 6.70$ 

$$K_{post} = \frac{1.49}{0.0342}, (5646.9), (6.70)$$

Conveyance = 8,088 cfs

Kpost ( Kpre

... Compensation Needed to keep 100-yr flood flow from decreasing.

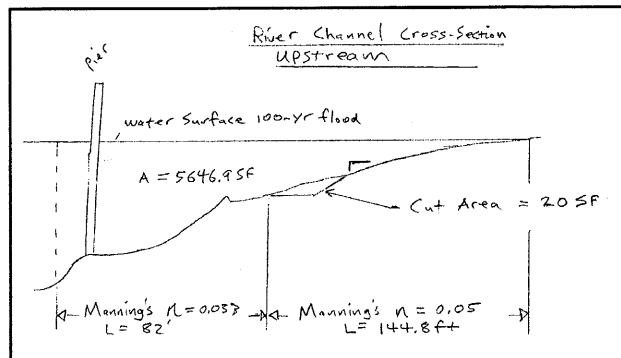


EXPIRES: 12/31/2021

		Butteville Landing		2/7
	SDW	Conveyance & Compensation Cut	12/1/21	3/7
Job No.	Ву	Subject	Date	Sheet No.



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Designed Conveyance Compensation grand overbank Pier  $N = \frac{1.49}{10.0439} \cdot (227.2) + (0.05) \cdot (0.04) + (0.012)(99)$   $N = \frac{(0.0439) \cdot (227.2) + (0.05) \cdot (0.04) + (0.012)(99)}{326.2}$   $N = \frac{1.49}{10.0342} \cdot (0.05) \cdot (0.04) + (0.012)(99)$ 

A = 5,666,9 SF

WP= 82+144.8+99+0.4 WP= 326.2

R= 17.37

 $R^{2/3} = 6.71$ 

Kprop = 1.49 . 5666.9 . 6.71

Kprop = 1,656,640 CFS

Kprop Z Kpre OK! 1,656,640 > 1,656,421 CFS

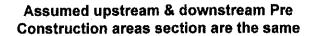


		·	EXPIRES: 12/31/2021	
	SDW	Butteville Landing Conveyance & Compensation Cut	12/1/21	4/7
Job No.	Ву	Subject	Date	Sheet No.

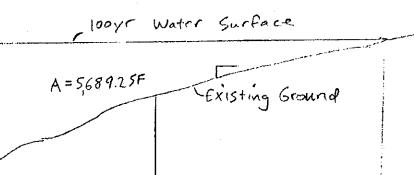


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River Channel Cross-Section



Mannings N = 0.033 Mannings N = 0.05 \_\_\_\_\_

# Pre Construction

 $n = \frac{(92') \cdot 0.033 + (144.8) \cdot 0.05}{226.8'}$ 

Wetted Perimeter, WP: Wetted.

Perimeter is the length in the

Cross-section that the Water

flows over causing resistance.

Perived in Civil 3D By Pline

WP = 226.8 ft

Kpre = 1.49/0.0439 . (5689.2) . 8.57

Kpre = 1,656, 421 cfs



Job No.	SDW By	Butteville Landing  Conveyance & Compensation Cut  Subject
---------	-----------	--

5/7 11/17/21 Date

Sheet No.



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#### **DownStream**

# Post Construction

Kpost = 1.4% A R's

$$N_{avg} = \frac{225.8'(6.044) + 125.0'(6.012)}{350'.8''}$$

$$N_{avg} = 0.0326$$

WA = 350.8 ft = 225.8+125.0

$$R = 16.04$$

$$R = 6.36$$

Kpost & Kpre

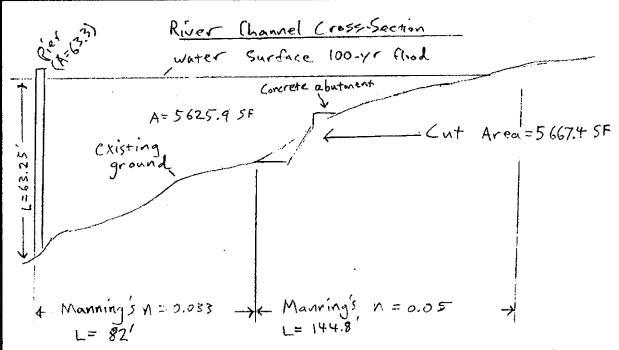
.. So, compensation is needed to keep loo-yr flood flow from decreasing.



		Butteville Landing		
	SDW	Conveyance & Compensation Cut	11/17/21	6/7
Job No.	Ву	Subject	Date	Sheet No.



2613 12th ST SE, SALEM, OREGON 97302 civil engineers . land surveyors (503) 363-9225



Designed Conveyance Compensation Channel overbank Steel Pilings Kprop = 1.49, A R<sup>2/3</sup>

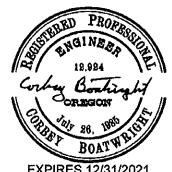
N = (0.033) 81'+ (0.05).144.8'+ (0.05) (0.44+(0.012).125  $N_{\text{avg}} = \frac{(0.033)81 + (0.05) \cdot 144.8 + (0.05)}{351.2}$ A = 5625.9 + 41.55F = 5667.4 sf  $N_{avg} = 0.032.55$  WP = 82'-1' + 144.8' + 125+0.4 = 351.2

R<sup>2/3</sup> = 6.386 Kprof = 1.49 · 5667.4 · 6.386

Kprop= 1,656,716.0CFS

Kprop 2 Kpre OK!

1,656,716. 2 1,656,421. CFS



EXPIRES 12/31/2021

		Buttaville Landing		
	SOW	Conveyance & Compensation Cut	11/17/21	7/7
Job No.	Ву	Subject	Date	Sheet No.

